#### STORMWATER REPORT

# 20 LEDIN AVENUE REDEVELOPMENT WASTE MANAGEMENT OF MASSACHUSETTS, INC. 20 LEDIN AVENUE AVON, MASSACHUSETTS

## **Prepared For:**

## WASTE MANAGEMENT OF MASSACHUSETTS, INC. 26 PATRIOT PLACE FOXBOROUGH, MASSACHUSETTS 02035

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CEC Project 311-399



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#### 1.0 PROJECT NARRATIVE

#### 1.1 INTRODUCTION

On behalf of Waste Management of Massachusetts, Inc. (the "Applicant"), Civil & Environmental Consultants, Inc. (CEC) has prepared this stormwater report and analysis to demonstrate compliance with the Massachusetts Department of Environmental Protection (MassDEP) Stormwater Management Standards, in accordance with the Massachusetts Wetlands Protection Act Regulations (310 CMR 10.00) and the Town of Avon Zoning Bylaws. This Stormwater Management Report describes the proposed design as depicted on the Site Plans prepared by Civil & Environmental Consultants, Inc., dated April 23, 2021, provided under separate cover.

The applicant is proposing to redevelop an existing 2.3-acre parcel of land located at 20 Ledin Avenue in Avon, Massachusetts (the "Site") in order to expand an existing building by  $\pm 17,120$  square feet (sf) along with associated landscape and utility infrastructure improvements (the "Project").

#### 1.2 EXISTING CONDITIONS

The 2.3-acre parcel of land, located along Ledin Avenue within the existing Avon Industrial Park, is currently used as an industrial space with an approximate  $\pm 0.75$  acre area of undeveloped land on the south side of the property, consisting of boulders, ledge, and a wooded area. The Site is bounded to the north by Ledin Avenue, to the south and east by developed industrial property, and to the west by an existing Waste Management of Massachusetts, Inc. industrial property. See Figure 1 for a Site Location Map and Figure 2 for an Aerial Site Plan.

Under existing conditions, approximately one-half of the Site (1.2-acres) consists of impervious areas including the existing building as well as walkways and the paved parking lot. The remaining area is approximately one-third grassed areas and two-thirds undeveloped land comprised of boulders and wooded areas.

## 1.2.1 Topography

Existing topography within the Site ranges from elevation 249 (NGVD 29) in the southwest corner of the property to elevation 226 ft. in the southeast corner of the property by the easterly edge of the property near the existing off-site wetland, located on the adjacent property of 10 Ledin Avenue. The developed portion of the site generally pitches away from the building from west to east at a slopes between approximately two (2) to six (6) percent, while the undeveloped portion pitches from west to east at a slope of approximately ten (10) percent for about two-thirds of the area and then slope down to the wetland area at the easterly property boundary at an approximate 2 horizontal to 1 vertical grade.

#### 1.2.2 Flood Zones

The Site is not located within a flood zone as shown on the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) for the Town of Avon, Map 25021 C0218E effective July 17, 2012. Refer to Figure 3.

#### 1.2.3 Wetlands

A wetlands investigation was performed by Lucas Environmental, LLC in July 2019. The result of the investigation indicated that a wetland resource area is present to the southeast of the Site on an adjoining property. The wetland area is shown on the Site Plans included under separate cover, and a more detailed description of the wetland areas is included in the Notice of Intent under separate cover.

#### 1.2.4 Geotechnical

According to the Natural Resources Conservation Service (NRCS) Web Soil Survey, the soils within the Site are classified as Canton fine sandy loam (#422B) and Urban land (#602).

The Canton fine sandy loam is identified as extremely stony and is comprised of Charlton soils, which are characterized as well drained soils derived from loamy melt-out till, Montauk soils, which are characterized as well drained soils derived from lodgment or flow till derived primarily from granite, gneiss, and/or schist, and Scituate soils, which are characterized as moderately well

drained soils formed in a loamy eolian influenced mantle of till underlain by sandy lodgement till. These mapped soils are classified as Hydrologic Soils Group (HSG) B.

The Urban land is identified by the NRCS as "areas where 85% of the land surface is covered by structures or impervious surfaces such as buildings, pavement, industrial site, and railway yards. Full identification of the underlying soil was not possible in the mapping process."

Additionally, BSC Group conducted a subsurface evaluation in 2003 in support of a septic system repair at the Site. Five test pits were excavated at the Site including two in the northeast quadrant adjacent to the property line and three in the central southern portion of the site. All of the borings, once below pavement, gravel and fill materials, encountered a sandy loam with loose cobbles and stones. Refusal was found between approximately 5-feet below grade to 8-feet below grade. Groundwater was not encountered at any of the borings. For the purpose of determining the separation from groundwater for proposed stormwater infiltration practices, where no groundwater was observed, the groundwater was assumed to be located at the bottom of the borings or bedrock. Refer to Appendix B for the supporting information including the test pit logs.

For the purposes of the hydrologic analysis, the soils identified within this area were classified as HSG B based on surrounding soils and previous test pits performed by others. For the purpose of the stormwater management design, the soils were assumed to be classified as "sandy loam", which has an infiltration rate of 1.02 inches per hour based on the Rawl's rates as identified in the Massachusetts Stormwater Management Handbook.

#### 1.3 PROPOSED PROJECT

As previously noted, the Project includes the expansion of an existing building, consisting of a  $\pm 17,120$  sf building, along with associated site, landscape and utility infrastructure improvements. The Project is proposed within an existing industrial park and is consistent with the Town of Avon zoning and intended land-use for the Site. The Project will include new water quality and quantity controls designed to protect surface and groundwater resources and adjacent properties from

<sup>&</sup>lt;sup>1</sup>National Cooperative Soil Survey. (2009). *Soil Survey of Middlesex County, Massachusetts*. Natural Resources Conservation Service.

In the proposed condition, approximately 86% of the Site will be impervious consisting of paved parking areas, sidewalks and building roof areas. The remainder of the Site will consist of landscaped areas. The overall drainage patterns on the Site will be maintained in the proposed condition with the grades generally consistent with the original grades in the central portion of the Site. Stormwater runoff from the paved driveways and sidewalk areas will be directed to water quality units with inlets providing sediment removal as well as oil and gas protection. The stormwater will be conveyed to additional water quality best management practices providing additional water quality treatment prior to infiltration. The roof runoff and a portion of the rear parking areas will be routed to subsurface infiltration chambers where groundwater recharge will be provided. Outlet control structures are proposed that will divert stormwater flows in excess of the infiltrative capacity of the chambers to the municipal stormwater system located in Ledin Avenue. The proposed design will reduce the peak rate of runoff from the Site, increase the quality of water leaving the Site, and provide additional recharge. Furthermore, the water quality units within the Site have been designed to provide the required 80% TSS removal for the stormwater runoff from the impervious pavement areas from the adjacent property that are draining into the Site.

#### 2.0 STORMWATER MANAGEMENT SYSTEM

#### 2.1 DESCRIPTION OF RUNOFF CONTROLS

The stormwater management improvements consist of components designed to manage runoff from the Site. These components attenuate runoff discharge peaks, minimize erosion, minimize the transport of sediments, improve water quality, and prevent impacts to the municipal drainage system and any downstream resource areas.

The stormwater management system implements a treatment drain of the Best Management Practices designed to provide 80% TSS (Total Suspended Solids) removal for stormwater runoff from the proposed drive aisles and parking areas. The proposed stormwater management system will use the following specific control measures:

Proprietary particle separators (Stormceptor® water quality units): The proposed Stormceptor water quality units provide efficient removal of free oils, debris and total suspended solids (TSS). Although not the main objective of the water quality unit some removal of heavy metals and other nutrients is also achieved. Water quality units allow for safe and easy removal of collected material and should be inspected and cleaned in accordance with the Operations and Maintenance (O&M) Plan and per manufacturer's recommendations. See the Long Term Pollution Prevention and O&M Plan included in Section 6 and Appendix C for supporting information.

The use of these units for treatment of stormwater is accepted as a good practice and is in accordance with sound professional standards. A Massachusetts Stormwater Evaluation Project (MASTEP) Technology Review has been performed for the Stormceptor® affirming testing methods are acceptable for achieving the pollutant removal efficiencies noted<sup>2</sup>. See Appendix C for the MASTEP Technology Review.

University of Massachusetts – Amherst, Stormwater Technologies Clearinghouse http://www.mastep.net/database/data.cfm (accessed October 2014)

Stormwater Infiltration Chambers (StormTech® MC-3500 chambers) with Isolator Row:

The Isolator Row will provide efficient removal of free oils, debris and total suspended

solids (TSS) as an added level of pretreatment of the stormwater runoff. The Isolator Rows

allow for safe and easy removal of collected material and should be inspected and cleaned

in accordance with the O&M Plan and per manufacturer's recommendations.

Stormwater recharge for the proposed redevelopment is provided through the infiltration

treated runoff from the pavement areas and clean runoff from the building's roof areas via

the StormTech® MC-3500 chambers which are located beneath the paved parking and

circulation areas.

The use of Isolator Rows for treatment of stormwater is accepted as a good practice and is

in accordance with sound professional standards. A Massachusetts Stormwater Evaluation

Project (MASTEP) Technology Review has been performed for the Stormtech Isolator

Row affirming testing methods are acceptable for achieving the pollutant removal

efficiencies noted. See Appendix C for the MASTEP Technology Reviews and supporting

information.

All of these proposed runoff controls are detailed on the Site Plans included in Appendix D.

2.2 CONSTRUCTION SEQUENCE PLAN

The purpose of the Construction Sequence Plan is to develop a working schedule for the

implementation of the proposed stormwater improvements.

Prior to initiating any work, the siltation control barriers will be installed along the limit of work.

Once the appropriate permits are obtained, the construction project will commence in the following

sequence:

1. Install all necessary erosion and siltation barriers as shown on the design drawings and

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install temporary fencing as needed.

2. Perform clearing and stripping of the Site, stockpiling materials to be re-used for

Civil & Environmental Consultants, Inc.

20 Ledin Avenue Redevelopment April 2021 earthwork activities.

- 3. Perform excavation for building foundation areas and subsurface utilities.
- 4. Install proposed utilities and stormwater infrastructure and construct building foundations.
- 5. Place clean fill/pavement base materials and install pavement base and curbing.
- 6. Construct buildings.
- 7. Install proposed final landscaping.
- 8. Remove existing erosion control measures.

All construction water will be collected and treated in accordance with the Erosion and Sediment Control Plan included in Section 5.0.

#### 3.0 STORMWATER ANALYSIS

#### 3.1 METHODS OF ANALYSIS

A hydrologic analysis has been performed for the Site comparing existing conditions and post-development conditions using a software program developed by HydroCAD. This program analyzes site hydrology by the graphic peak discharge method documented in Technical Release No. 20 and Technical Release No. 55 published by the United States Department of Agriculture (USDA) Soil Conservation Service.

The following variables were developed for the contributing watersheds (drainage areas) in order to complete the analysis:

- Rainfall Depth: A hydrologic analysis was performed for the 24-hour 2-year, 10-year, 25-year, and 100-year, Type III storm events (3.2, 4.7, 5.5, and 6.7 inches respectively) for each drainage area. The rainfall depths for the study area were obtained from available charts published in Technical Paper No. 40.
- Runoff Curve Number (RCN): The RCN is a hydrologic characteristic that contributes to the peak rate of runoff and volume from a given storm event. It is dependent upon soil conditions and land use. Generally, higher curve numbers are associated with less pervious soils and, hence, greater amounts of runoff. As previously noted, based on the geotechnical investigation, the soils consist of Hydrologic Soil Group (HSG) B and was used accordingly in determining RCNs.
- Time of Concentration: The time of concentration is defined as the time it takes runoff to travel from the hydraulically most distant part of the watershed to the downstream point of interest. This parameter is dependent on the characteristics of the ground surface and condition of the travel path. Times of concentration were calculated for the various sub catchments using the HydroCAD program, with a minimum time of concentration of six (6) minutes used in accordance with the protocol outlined in Technical Release No. 55.

#### 3.2 DRAINAGE AREAS

In order to perform the analysis, the contributing drainage areas for pre-development, existing, and post-development conditions were delineated. The delineation of the drainage areas were determined by the topography depicted on the Existing Conditions plan based on the topographic field survey performed in March 2019, with supplemental data collected in July 2019. Brief descriptions of the existing conditions and proposed conditions drainage areas are as follows:

- Existing Conditions: The Site is divided into three (3) drainage areas and the stormwater flows to two (2) design points, which are identified as the municipal drainage system on Ledin Avenue flowing to the northeast and the neighboring property to the east. Refer to Figure HYD-EX for the existing conditions drainage areas. The descriptions of the existing conditions drainage areas are listed below:
  - Subcatchment 1A-EX is the ±2.0-acre front portion of the property that drains towards Ledin Avenue and an existing catch basin located within the roadway. The drainage area is comprised of gravel, grassed areas, roof and paved areas. Stormwater from this drainage area drains overland and untreated into the municipal stormwater system.
  - Subcatchment 1OFF-EX is the ±1.49-acre area that drains into the Site from the adjacent property, 40 Ledin Avenue. The drainage area is comprised of roof areas, pavement and brush areas. Stormwater from this drainage area flows overland and untreated from the adjoining property onto the Site. It is collected by a catch basin located in the southeast corner of the Site and conveyed into the municipal stormwater system in Ledin Avenue. The catch basin also collects stormwater from sub catchment 1A-EX.
  - O Subcatchment 2A-EX is the  $\pm 0.34$ -acre undeveloped, southeast portion of the property that is comprised of woods and brush. Stormwater from this drainage area flows overland and untreated to the east to the adjoining property. This drainage area is adjacent to the wetlands to the south and east of the Site.

TABLE 3.1 EXISTING CONDITIONS									
Drainage Area Discharge Location Design Point Area (ft²) Curve Number¹ Concentration (minutes)									
1A-EX	т 1. т	1	85,204	86	6.0				
10FF-EX	Ledin Avenue	1	64,730	97	6.8				
2A-EX	Adjoining Property	2	14,724	61	6.0				

#### Notes:

- 1. Curve number refers to the weighted curve number than encompasses the varied terrain, and associated individual curve number values, within the drainage area.
- 2. A minimum time of concentration of 6 minutes was used if a time of concentration of less than 6 minutes was determined when evaluating the drainage area.
- **Proposed Conditions:** The Site is divided into five (5) drainage areas and the stormwater flows to one (1) design point, which is identified as the municipal drainage system in Ledin Avenue flowing to the northeast. Refer to Figure HYD-PR for the proposed conditions drainage areas. The descriptions of the proposed conditions drainage areas are listed below:
  - Subcatchment 1A-PR is the ±0.61-acre front portion of the property that drains towards Ledin Avenue and an existing catch basin located within the roadway. The drainage area is comprised of gravel, grassed areas and paved areas. Stormwater from this drainage area drains overland into the municipal stormwater system in Ledin Avenue.
  - o Subcatchment 1B-PR is the ±0.21-acre area along the westerly side of the proposed building, consisting of grassed and paved areas that drain into the proposed catchbasins in the southwest portions of the Site, routed to a proprietary water quality unit and conveyed into the municipal stormwater system in Ledin Avenue. A portion of Subcatchment 1OFF-EX also drains to the catch basins located in Subcatchment 1B-PR.

- Subcatchment 1C-PR is the ±0.97-acre roof area of the existing and proposed building expansion roof areas. Runoff collected from this area will be conveyed to the subsurface chambers where it will recharge into the groundwater. Flows exceeding the design capacity of the chambers will be directed into the Ledin Avenue municipal stormwater system.
- o Subcatchment 1D-PR is the  $\pm 0.50$ -acre paved and grassed area located in the southern portion of the site. Runoff collected from this area will be collected in deep sump hooded catch basin, routed to a water quality unit and conveyed to the subsurface chambers where it will recharge into the groundwater. Flows exceeding the design capacity of the chambers will be directed into the Ledin Avenue municipal stormwater system.
- Subcatchment 10FF-EX is the ±1.49-acre area that drains from the adjacent property, 40 Ledin Avenue. This areas will remain unchanged in the proposed condition. The drainage area is comprised of a roof areas, brush, and pavement. Stormwater from this drainage area flows overland and untreated from the adjoining property onto the Site. The runoff from this subcatchment is collected via deep sump hooded catch basins within the Site, routed to the proprietary water quality unit, and conveyed to the municipal drainage system in Ledin Avenue.

TABLE 3.2										
POST-DEVELOPMENT CONDITIONS										
Drainage Area	Curve Number <sup>1</sup>	Time of Concentration (minutes) <sup>2</sup>								
1A-PR			26,398	93	6.0					
1B-PR		1	9,191	76	6.0					
1C-PR	Ledin Avenue		42,427	98	6.0					
1D-PR			21,919	96	6.0					
10FF-PR			64,730	97	6.8					

#### 3.3 RESULTS OF ANALYSIS

A stormwater analysis was performed for the 2-year, 10-year, 25-year, and 100-year storm events in order to determine that there will be no increase in stormwater runoff once the proposed construction is complete and the stormwater control structures are in place. Detailed calculations are attached in Appendix A. The points of compliance for existing, and post-development conditions are the two design points noted above. A summary of the peak stormwater runoff and volumes is provided below.

TABLE 3.3 PROJECT STORMWATER RUNOFF RATES												
	Runoff Rate (cfs)											
	2-Y	Year 10-Year			25-Year		100-Year					
	Ex.	Prop.	Ex.	Prop.	Ex.	Prop.	Ex.	Prop.				
1	8.48	7.54	13.56	12.09	16.28	15.96	20.35	19.03				
2	0.11	-	0.41	-	0.61	-	0.94	-				

As shown in Table 3.3, runoff from post-development runoff rates in Ledin Avenue do not exceed existing runoff rates and the runoff to the adjacent property has been eliminated. Supporting calculations are provided in Appendix C.

#### 3.3.1 Hydrology

The proposed drainage infrastructure, consisting of deep sump hooded catch basins, water quality units, manholes and subsurface groundwater chambers have been designed to convey storm events up to and including the 25-year storm event.

#### 4.0 STORMWATER CONTROL SYSTEM DESIGN CRITERIA

#### 4.1 MASSDEP STORMWATER MANAGEMENT POLICY

Stormwater discharges from the proposed Project is subject to the Massachusetts DEP Stormwater Management Policy (the Policy). The Policy is designed "to protect the wetlands and waters of the Commonwealth from adverse impacts of storm water runoff." To accomplish this goal, the Policy establishes ten (10) performance standards to control stormwater quantity and quality. These standards establish the level of required controls which can be achieved through the use of site planning, structural and non-structural controls, and other best management practices (BMPs). The Stormwater Checklist is provided in Appendix A. Stormwater modeling methodology is discussed in detail in section 3.0. Results of the stormwater modeling of the existing and proposed conditions are provided as Appendix C

## 4.1.1 Stormwater Management Controls

The following section documents compliance with the MassDEP Stormwater Management Standards.

#### Standard 1

No new stormwater conveyances (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

The project is designed so that there are no new stormwater conveyances that could discharge untreated stormwater into, or cause erosion to, wetlands or waters of the Commonwealth. The proposed project generally retains the overall drainage patterns of the pre-development conditions and no discharges to wetlands are proposed.

#### Standard 2

Stormwater management systems must be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates.

The total post-development peak discharge rates do not exceed pre-development rates for the 2, 10, 25 and 100-year storm events. Stormwater modeling methodology is discussed in detail in Section 3.0. The model output is provided in Appendix C. The results are provided above in Table 3.3.

#### Standard 3

Loss of annual recharge to groundwater should be minimized through the use of infiltration measures to the maximum extent practicable. The annual recharge from the post-development site should approximate the annual recharge from the pre-development or existing site conditions, based on soil types.

The project is designed to comply with this criteria. The project will result in the addition of approximately 32,983 square feet of new impervious areas. In accordance with the stormwater standards, 0.35-inches of recharge must be provided for the increase in impervious areas on the Site for HSG B soils. Accordingly, a total of 962 cubic feet (cf) of groundwater recharge is required based on the increase of impervious areas. Through the introduction of the various stormwater infiltration practices, a total of 2,011 cf of recharge is proposed, providing significantly more recharge than the regulatory requirement.

Based on the conservative infiltration rate of 1.02 inches per hour utilized in the analysis, each of the infiltration systems has been designed to provide the drawdown of all stormwater below the low flow outlets in less than 72 hours. Supporting calculations are provided in Appendix C.

#### Standard 4

For new development, stormwater management systems must be designed to remove 80% of the average annual load (post-development conditions) of Total Suspended Solids (TSS). It is presumed that this standard is met when:

- A. Suitable nonstructural practices for source control and pollution prevention are implemented;
- B. Stormwater management best practices (BMPs) are sized to capture the prescribed runoff volume; and

C. Stormwater management BMPs are maintained as designed.

The proposed development utilizes several methods of storm water management to reduce TSS

generation including deep sump hooded catch basins, proprietary water quality units, StormTech

Isolator Rows, Subsurface Infiltration Chambers, consistent with the Policy. The estimated TSS

removal rate from the proposed BMP treatment train for each system exceeds the 80%

requirement. Supporting calculations can be found in Appendix C.

The Site will include vehicle and equipment storage and may be classified as a Land Use with

Higher Potential Pollutant Loads (LUHPPL). Accordingly, the proposed stormwater management

system has been designed to treat the 1" Water Quality Volume and provide 44% TSS removal

pre-treatment prior to infiltration. Supporting calculations can be found in Appendix C.

A comprehensive Operations and Maintenance Plan (O&M) has been developed and is included

in Section 6.0 of this report.

Standard 5

Stormwater discharges from areas with higher potential pollutant loads require the use of specific

stormwater management BMPs. The use of infiltration practices without pre-treatment is

prohibited.

The Site may be classified as a Land Use with Higher Potential Pollutant Loads (LUHPPL).

Accordingly, the proposed stormwater management system has been designed to treat the 1" Water

Quality Volume and provide 44% TSS removal pre-treatment prior to infiltration. Pretreatment is

provided by deep sump hooded catch basins and proprietary water quality units prior to discharge

to the infiltration chambers. Pre-treatment is provided by deep-sump hooded catch basins and the

StormTech Isolator Row prior to discharge to the subsurface Infiltration Chambers. Supporting

calculations can be found in Appendix C.

Standard 6

Stormwater discharges to critical areas must utilize certain stormwater management BMPs approved for critical areas. Critical areas are Outstanding Resources Waters (ORWs), shellfish beds, bathing beaches, cold water fisheries, and recharge areas for public water supplies.

The project does not discharge to critical areas.

Standard 7

Redevelopment of previously developed sites must meet the Stormwater Management Standards to the maximum extent practicable. Where it is not practicable to meet all the Standards, new (retrofitted or expanded) stormwater management systems must be designed to improve existing conditions.

The project fully complies with the Stormwater Standards.

Standard 8

Erosion and sediment controls must be implemented to prevent impacts during construction, or land disturbance activities.

Erosion and sediment controls are integral to the project improvements. The plan includes compost silt socks which will be installed down-gradient of the proposed work area and silt sacks which will be installed in existing catch basins within the adjacent rights of way. A preliminary Erosion and Sediment Control Plan has been developed and is included in Section 5.0 of this report. A detailed Stormwater Pollution Prevention Plan will be prepared and a Notice of Intent will be submitted to the United States Environmental Protection Agency prior to commencement of construction activity. Measures will be utilized throughout construction to prevent erosion, control sediments, and stabilize exposed soils as discussed in Section 5.0.

Standard 9

All stormwater management systems must have an operations and maintenance plan to ensure that systems function as designed.

5.0 CONSTRUCTION PERIOD POLLUTION PREVENTION AND SEDIMENTATION

AND EROSION CONTROL PLAN

5.1 INTRODUCTION

The greatest potential for sediment generation will occur during the construction. An extensive

erosion and sedimentation program is proposed and will be diligently implemented during

construction of the project. The erosion control program will minimize erosion and sedimentation

that could potentially impact resources areas. Water quality will be maintained by minimizing

erosion of exposed soils and siltation. Erosion control barriers will be installed and exposed soil

areas re-vegetated as soon as possible after work in an area is completed.

This Erosion and Sediment Control Plan includes preliminary measures and requirements for

management and implementation of erosion and sediment controls during construction. A detailed

Stormwater Pollution Prevention Plan (SWPPP) will be prepared and a Notice of Intent (NOI) will

be filed with the United States Environmental Protection Agency (USEPA) in accordance with

USEPA's National Pollutant Discharge Elimination System (NPDES) General Permit program for

stormwater discharges from construction sites prior to the commencement of any construction

activity. The SWPPP will contain elements from this Erosion and Sediment Control Plan and will

include additional and more detailed inspection and maintenance procedures and will include

maintenance logs, forms and additional erosion and sediment control measures.

**Responsible Party for Plan Compliance:** 

Waste Management of Massachusetts, Inc.

26 Patriot Place

Foxborough, Massachusetts 02035

**Emergency Contact Information:** 

To be determined.

A comprehensive Operations and Maintenance Plan (O&M) has been developed and is included in Section 6.0 of this report.

## Standard 10

All illicit discharges to the stormwater management system are prohibited.

There are no illicit discharges at the Site.

#### 5.2 CONSTRUCTION PHASE EROSION CONTROL MEASURES

The adjacent resource areas will be protected during construction by implementing siltation control measures, including the placement of compost silt socks as close as feasible to the down gradient limit of construction activity. The project may also implement other stabilization methods such as erosion netting and hydro seeding.

## 5.2.1 Short and Long Term Goals and Criteria

Short and long term goals will include a variety of stabilizing sediment and erosion controls around the limit of work. All construction-phase erosion and sediment controls have been designed to retain sediment on-site to the extent practicable and limit runoff and the discharge of pollutants (sediment) from exposed areas of the Site.

All control measures will be installed and maintained in accordance with the manufacturer's specifications and good engineering practices. Weekly inspections and routine monitoring will be used to determine the effectiveness of controls in use.

Litter and solid construction debris potentially exposed to the stormwater will be prevented from becoming a pollution source through routine monitoring and the use of laborers to "pick" as necessary.

#### 5.2.2 Stabilization Practices

The construction site activities will include numerous stabilizing practices. Sediment and erosion controls such as erosion netting, mulching and hydro-seeding may act as interim practices. Erosion netting material may include single net straw blankets or coconut blankets. Permanent stabilization practices will include the use of a hydro-seeding over vegetative support soil where additional exposure threatens stormwater quality. Seeding will be carried out with a seed mixture equal to the "Roadside Slope Mix" included below. All siltation barriers will remain in place until all exposed areas are re-vegetated.

## PLANTING SCHEDULE FOR EXPOSED AREAS

- 1. All exposed areas will receive 6 inches of topsoil or compost material.
- 2. Seed will be equal to "Roadside Slope Mix" as specified by the Mass. Highway Department. Please refer to chart below for specifications. This mixture will be spread at a rate of 5 pounds per 1,000 square feet.

TABLE 5.1 ROADSIDE SLOPE MIX									
Germination Purity Common Name Proportion Minimum Minimum									
Creeping Red Fescue	50%	85%	95%						
Kentucky 3	30%	85%	95%						
Domestic Rye	10%	90%	98%						
Red Top	5%	85%	92%						
Ladino Clover	5%	85%	96%						

#### 5.2.3 Structural Practices

Perimeter controls will consist of compost silt socks. In order to ensure effective performance, proper installation is required. 2" x 2" wooden stakes will be positioned on the downhill side (away from the job Site) of the silt socks. The posts will be driven at least one foot into the ground.

If deemed necessary after construction begins, a wash pad may be included to wash off vehicle wheels before leaving the Site.

## 5.3 NON-STRUCTURAL CONTROLS

## 5.3.1 Good Housekeeping

Non-structural controls are as effective as structural controls in sediment control. Non-structural controls to be used at the construction Site include:

• Regular sweeping of paved surface; and,

• Prompt cleanup of any waste or spilled waste materials.

#### 5.3.2 Exposure Minimization

Exposure will be minimized by providing both permanent and temporary soil stabilization (see Section 5.2.2) over areas that have been completely constructed, or areas that will not be revisited within a 30 day period.

Where practicable, industrial materials and activities will be protected from exposure to rain, snow, snowmelt, or runoff.

#### 5.3.3 Preventative Maintenance

A preventative maintenance program includes the timely inspection and maintenance of stormwater management devices. Examples of preventative maintenance include:

• Removal of obstructions, if any, from inlets and outlets.

• Removal of accumulated sediment and vacuuming water from sumps.

• Repairing and re-planting slope areas that experience erosion.

#### 5.3.4 Inspections

An experienced Construction Monitor will conduct inspections of construction areas once every 7 calendar days and within 24 hours of the occurrence of a storm event of 0.25 inches or greater, or the occurrence of runoff from snowmelt sufficient to cause a discharge. Storm event information from a weather station representative of the Site's location may be used to determine if a storm event of 0.25 inches or greater has occurred on the Site. Total rainfall will be measured for any day of rainfall during normal business hours that measures 0.25 inches or greater. Construction areas an experienced Construction Monitor will inspect include:

• Disturbed areas of the construction Site that have not been finally stabilized,

- Areas used for storage of materials that are exposed to precipitation,
- Structural control measures,
- Locations where vehicles enter or exit the Site, and
- The stormwater management system and discharge outlets.

Disturbed areas and areas used for storage of materials that are exposed to precipitation will be inspected for evidence of, or the potential for, pollutants entering the drainage system.

Sediment and erosion control measures identified will be observed to ensure that they are operating correctly. The discharge locations or points will be inspected to ascertain whether erosion control measures are effective in preventing significant impacts to receiving waters. Locations where vehicles enter or exit the Site will be inspected for evidence of offsite sediment tracking.

Based on the results of these routine inspections, the Contractor will correct any deficiencies found as soon as practicable. Results of the inspections, corrective actions taken in response to any deficiencies, and any opportunities for improvement that are identified will be documented in an inspection report.

#### 5.4 RECORDKEEPING

The following records will be maintained on the Site:

- 1. Dates when major grading activities occur,
- 2. Dates when construction activities temporarily or permanently cease on a portion of the Site,
- 3. Dates when stabilization measures are initiated, and
- 4. In addition, the following records will also be kept:
  - The Order of Conditions; and any additional permit conditions/approvals,
  - All inspection reports, and
  - Any spill reports.



## Table 5.2 - Construction BMPs Maintenance Log

Project Name: Ledin Avenue Building Expansion
Project Location: 20 Ledin Avenue, Avon, MA

Project Number: 311-399

Date: 4/22/2021 Prepared By: KPS Approved By: BG

Best Management Practice	Inspection Frequency	Date Inspected	Inspector	Minimum Maintenance and Key Items to Check	Cleaning or Repair Needed (List Items if Required)	Date of Cleaning or Repair	Performed by
Pavement Sweeping	To be monitored as needed			Paved areas within the active construction site can be swept on a regular basis to remove larger sediment particles from construction activities. Pavement areas adjacent to the Site will be swept if dirt and debris is tracked from the active construction site.			
Catch Basin Inlet Protection (Silt Sack Sediment Trap)	Inspect at least once every 7 calendar days or once every 14 calendar days and within 24 hours of the occurrence of storm event of 0.25 inches or greater.			Inspect for proper operation. If clogged, remove accumulated sediment and properly dispose of to maintain the capacity of the catch basin.			
Erosion Control Barrier (Compost Filter Socks and Silt Fence)	Inspect at least once every 7 calendar days or once every 14 calendar days and within 24 hours of the occurrence of storm event of 0.25 inches or greater.			Inspect for deterioration or failure. Remove sediment when buildup exceeds 6 inches or half the barrier height. The underside of straw bales should be kept in close contact with the earth and reset as necessary.			
Stabilized Construction Exit	Inspect at least once every 7 calendar days or once every 14 calendar days and within 24 hours of the occurrence of storm event of 0.25 inches or greater.			The exit shall be maintained in a condition that will prevent tracking of sediment onto public rights-of-way. The contractor shall sweep or wash pavement at exits which have experienced mud-tracking onto the pavement or traveled way. When wheel washing is required, it shall be done on an area stabilized with aggregate that drains into an approved sediment trapping device.  When the construction exit becomes ineffective, the stone shall be removed along with the collected soil material and redistributed on-site in a stable manner. The exit should then be reconstructed.  All sediment shall be prevented from entering storm drains, ditches, or waterways.			

## 6.0 OPERATIONS AND MAINTENACE (O&M) PLAN

#### 6.1 GENERAL

Stormwater management systems with multiple components, such as the one proposed for the Project, assures the cleanest possible discharges of stormwater to the environment. However, these systems must be routinely maintained to keep them in good working order. Additionally, this plan identifies potential sources of pollution that may affect the quality of stormwater discharges and describes the implementation of Long-Term Pollution Prevention practices to reduce potential pollutants in stormwater discharge. The party identified below will be responsible for the operation and maintenance of the stormwater management system and Site. Schedules and procedures for inspection and maintenance of the existing and proposed stormwater management system components are provided in the following sections.

#### **Responsible Party for Plan Compliance:**

Waste Management of Massachusetts, Inc.

26 Patriot Place

Foxborough, Massachusetts 02035

#### **Emergency Contact Information:**

To be determined

#### **Estimated O&M Budget:**

It is estimated that an annual budget of \$2,000 should be allocated to performing routine inspections and maintenance identified in this O&M Plan.

#### 6.2 ROUTINE INSPECTIONS

Inspections of the stormwater management system as a whole, and of the individual components of the system, will be carried out on a routine basis in accordance with the schedule identified in Section 6.3. Each will be inspected for sediment buildup, presence of oil, color and structural damage. The results of each inspection will be entered into an inspection log. Refer to Table 6.1 for the inspection log form.

#### 6.3 MAINTENACE PLAN

The Responsible Party incorporate a routine maintenance program to assure proper operation of the stormwater management system. Maintenance will be performed based on the results of inspections in accordance with the schedules identified in Table 6.1. The program will include the following maintenance activities:

## **Deep Sump Catch Basins**

- All catch basins shall be inspected a minimum of at least four times per year.
- Sediment, if more than two feet deep, and/or floatable pollutants shall be pumped from the basin and disposed of at an approved offsite facility in accordance with all applicable regulations.
- Any structural damage or other indication of malfunction will be reported to the site manager and repaired as necessary.
- During cleanings, confirm the oil/debris trap (hood) is installed properly, is free of clogs, and is functional. Reinstall or replace as needed.
- During colder periods, the catch basin grates must be kept free of snow and ice.
- During warmer periods, the catch basin grates must be kept free of leaves, litter, sand, and debris.

## **Water-Quality Structures**

- See the attached Manufacturer's instructions on operation and maintenance requirements and methodology.
- Inspect and clean twice per year or as required by manufacturer.
- Remove sediment and other trapped pollutants at the frequency or level specified by the manufacturer.

#### **Roof Drain Leaders**

- Perform routine roof inspections twice per year, typically in the spring and fall.
- Inspect for blockage and remove debris if required.
- Keep roofs clean and free of debris.
- Keep roof drainage systems clear.
- Keep roof access limited to authorized personnel.

## **Subsurface Infiltration System**

- See the attached Manufacturer's instructions on operation and maintenance requirements and methodology.
- Perform routine inspections on a monthly basis for the first three months after installation. Then, at a minimum, the treatment structure is to be inspected twice annually and the infiltrating structure is to be inspected annually.
- The subsurface infiltration system will be inspected twice during for the first year and annually thereafter by removing the manhole/access port covers and determining the thickness of sediment that has accumulated.
- If sediment is more than two inches deep, it must be suspended via flushing with clean water and removed using a vactor truck.
- Emergency overflow pipes will be examined at least once each year and verified that no blockage has occurred.

#### 6.4 LONG TERM POLLUTION PREVENTION MAINTENANCE

The Responsible Party incorporate a routine maintenance program to ensure the continued effectiveness of the structural water quality controls. Maintenance will be performed based on the results of inspections in accordance with the schedules identified below. The program will include the following maintenance activities:

#### **Maintenance of Pavement Systems**

Regular maintenance of pavement surfaces will prevent pollutants such as oil and grease, trash, and sediments from entering the stormwater management system. The following practices should be performed:

- Sweep or vacuum asphalt pavement areas quarterly with a commercial cleaning unit and dispose of removed material.
- Routinely pick up and remove litter from the parking areas, islands, and perimeter landscaping.

#### **Maintenance of Vegetated Areas**

Proper maintenance of vegetated areas can prevent the pollution of stormwater runoff by controlling the source of pollutants such as suspended sediments, excess nutrients, and chemicals from landscape care products. Practices that should be followed under the regular maintenance of the vegetated landscape include:

- Inspect planted areas on a semi-annual basis and remove any litter.
- Maintain planted areas adjacent to pavement to prevent soil washout.
- Immediately clean any soil deposited on pavement.
- Re-seed bare areas; install appropriate erosion control measures when native soil is exposed or erosion channels are forming.
- Plant alternative mixture of grass species in the event of unsuccessful establishment.
- Grass vegetation should not be cut to a height less than four inches.
- Pesticide/Herbicide Usage No pesticides are to be used unless a single spot treatment is required for a specific control application.
- Fertilizer usage should be avoided. If deemed necessary, slow release fertilizer should be used. Fertilizer may be used to begin the establishment of vegetation in bare or damaged areas, but should not be applied on a regular basis unless necessary.

#### Management of Snow and Ice

The Project has been designed such that snow stockpile areas can take advantage of the stormwater Best Management Practices (BMPs) proposed on the Site. Melting snow from the stockpiles will be collected by the site stormwater collection system, which will then be processed through a series of stormwater BMPs to remove sediment, debris and contaminants from the stockpiled snow. Snow stockpiles areas are not located within 100 feet of any open water body or regulated wetland resource area. Under no circumstances shall snow be disposed or stored in stormwater basins, ponds, rain gardens, swales, channels, or trenches.

Additionally, should significant snow fall events occur, which result in stockpiled snow impacting the operation of the Project Site, through the temporary loss of parking or limiting access in any way, the property manager may choose to have snow removed from the site. All snow removal

operations will be done in accordance with Massachusetts DEP guidelines BRPG01-01, effective date March 8, 2001.

#### 6.5 EMPLOYEE TRAINING

Training of personnel is essential to achieving proper operation and maintenance of the stormwater management system. Therefore, those Facility personnel who are responsible for operation and maintenance will be trained on the following subjects:

- Environmental laws and regulations relating to stormwater,
- The components and goals of the current Erosion and Sediment Control Plan,
- Site specific permit conditions and requirements,
- General Facility spill response procedures,
- General good housekeeping procedures, and
- General material management procedures.

Refresher training sessions will be held once a year following the completion of the Site Compliance Evaluation.



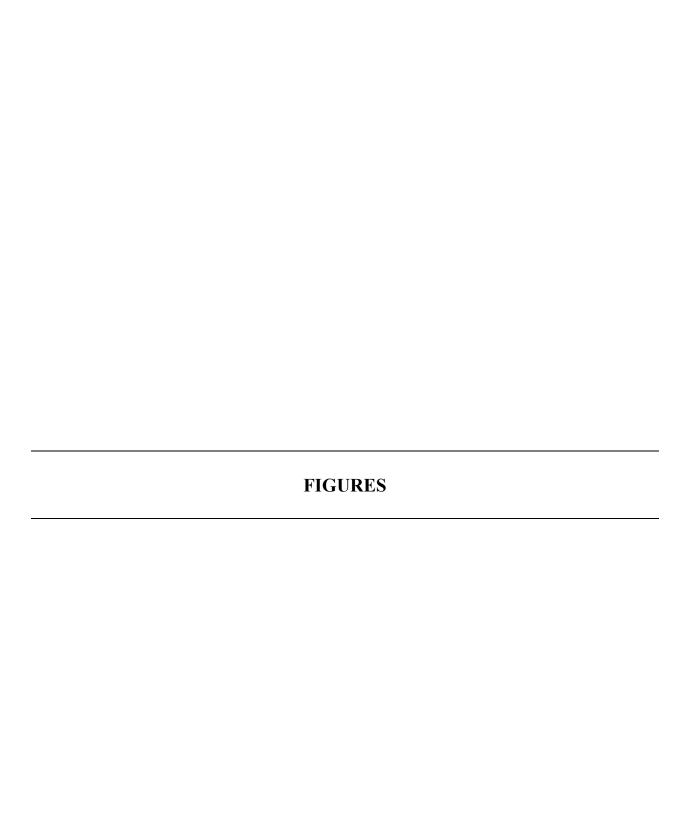
## Table 6.2 - Stormwater Operations and Maintenance Log

Project Name: Ledin Avenue Building Expansion
Project Location: 20 Ledin Avenue, Avon, MA

Project Number: 311-399

Date: 4/23/2021 Prepared By: DR Approved By: KPS

Best Management Practice	Inspection Frequency	Date Inspected	Inspector	Minimum Maintenance and Key Items to Check	Cleaning or Repair Needed (List Items if Required)	Date of Cleaning or Repair	Performed by
Deep Sump Catch Basins	Inspect four times per year. Clean four times per year, in the spring and fall, or whenever sediment buildup exceeds two (2) feet in depth.			Remove trash and deposits. During cleanings, confirm the oil/debris trap (hood) is installed properly, is free of clogs, and is functional. Reinstall or replace as needed. Take care not to damage the oil/debris trap (hood) during cleaning.			
Water Quality Structure	Inspect twice per year or as required by the manufacturer.			Clean twice per year or as required by the manufacturer.  Remove sediment and other trapped pollutants at the frequency or level specified by the manufacturer. No use of clamshell buckets without prior approval. Increase inspection frequency, as needed, based on observed sediment loading.			
Subsurface Infiltration System	Inspect monthly for the first three months. Then, at a minimum, the treatment structure is to be inspected twice annually and the infiltrating structure is to be inspected annually as required by the manufacturer.			Remove sediment once per year or when buildup exceeds two (2) inches in depth.			







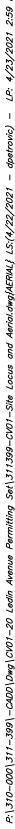
www.cecinc.com

20 LEDIN AVENUE REDEVELOPMENT

AVON, MASSACHUSETTS

SITE LOCATION MAP

DRAWN BY:	EMW	CHECKED BY:	DRAFT	APPROVED BY:	DRAFT	FIGURE NO.:	_
DATE:	APRIL 2021	DWG SCALE:	1"=2,000'	PROJECT NO:	311-399		1





311-399

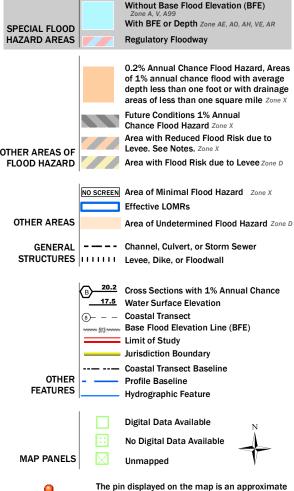
www.cecinc.com DRAWN BY: EMW CHECKED BY: DRAFT FIGURE NO.: DRAFT APPROVED BY: APRIL 2021 DWG SCALE: 1"=2,000' PROJECT NO: DATE:

# National Flood Hazard Layer FIRMette



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



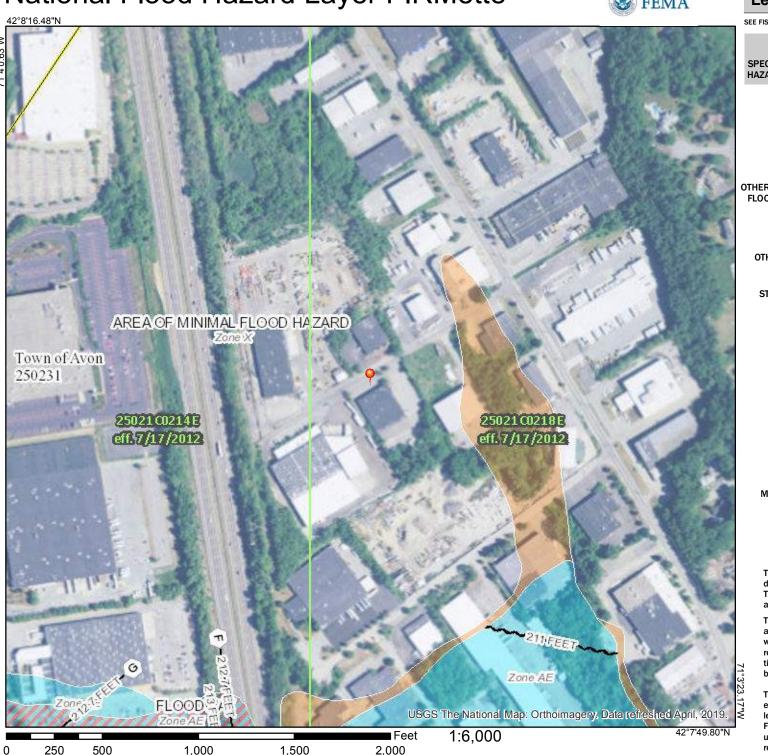


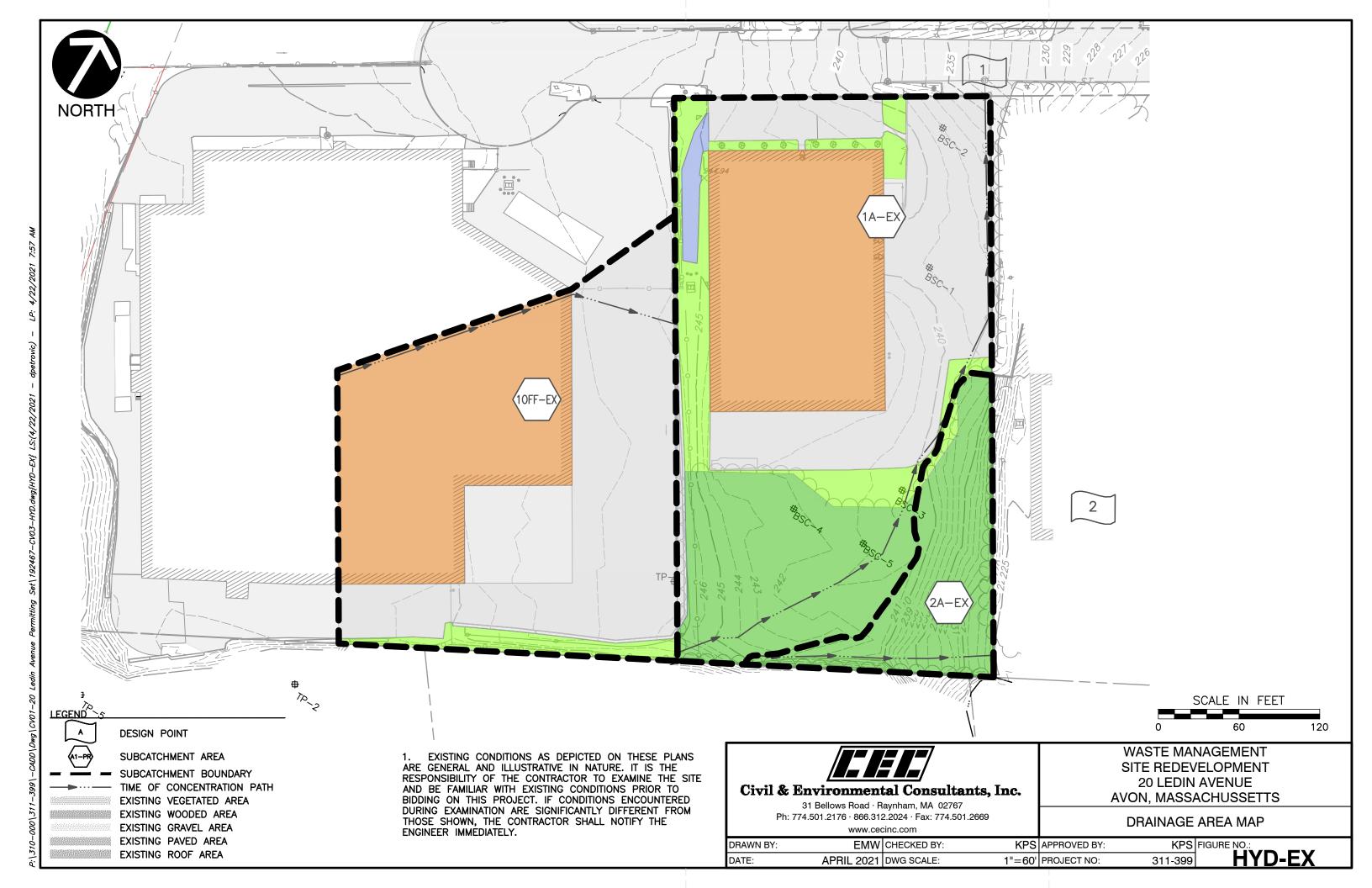
The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

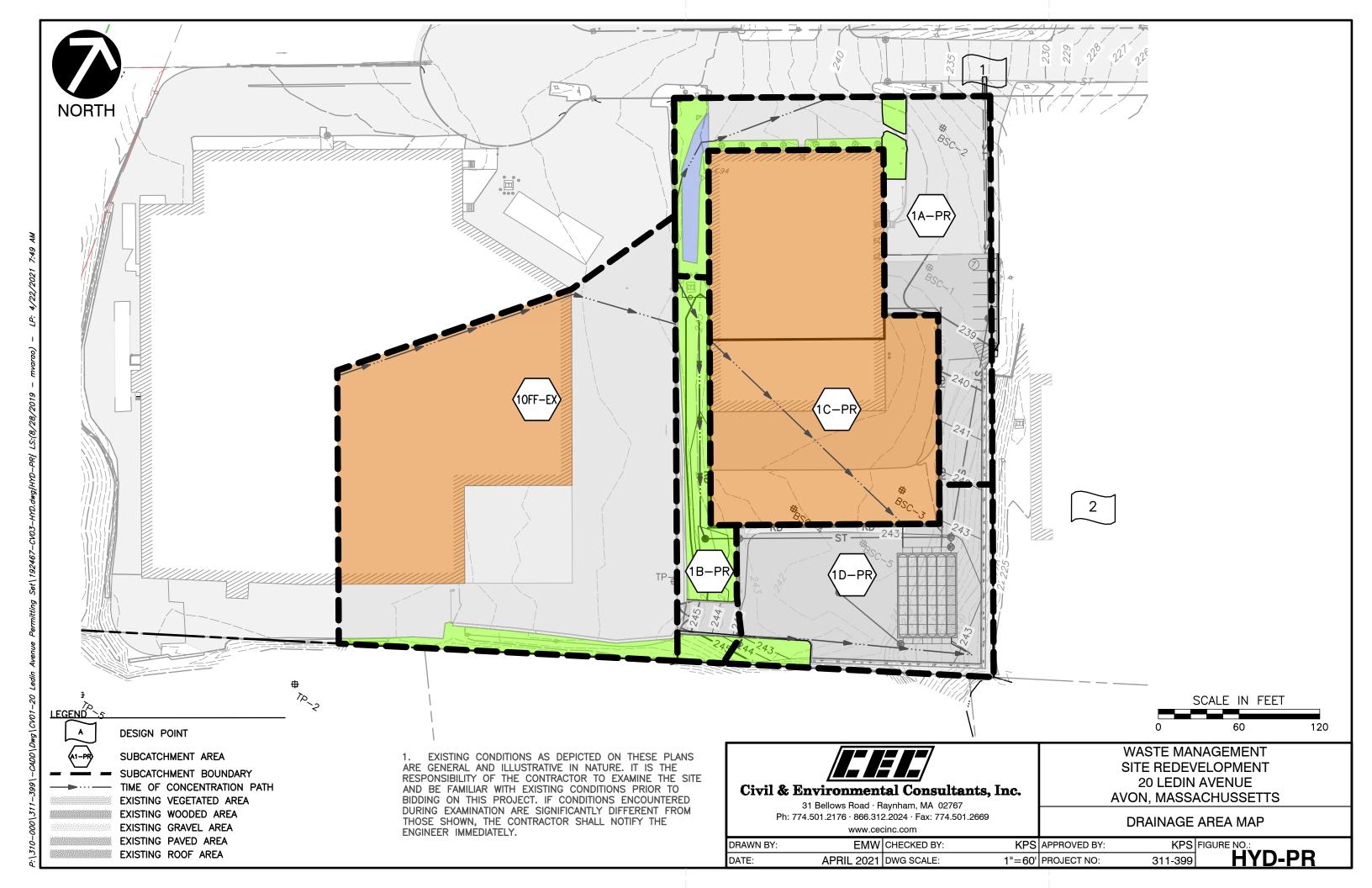
This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

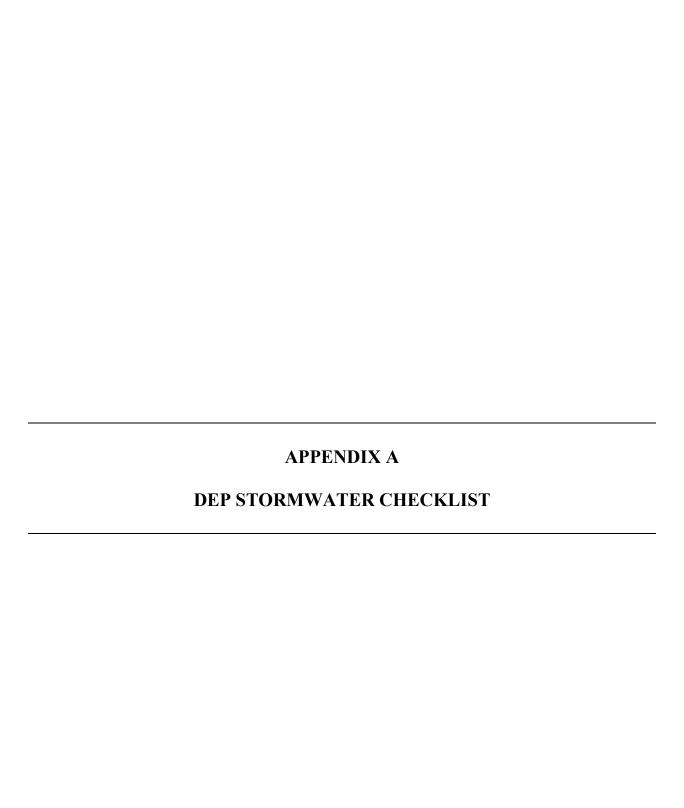
The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/11/2019 at 8:59:25 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.











## **Massachusetts Department of Environmental Protection**

Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

#### A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals. This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8<sup>2</sup>
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

<sup>&</sup>lt;sup>1</sup> The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

<sup>&</sup>lt;sup>2</sup> For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



#### **Massachusetts Department of Environmental Protection**

Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

#### B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

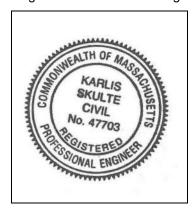
*Note:* Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

## **Registered Professional Engineer's Certification**

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



#### Checklist

	<b>expject Type:</b> Is the application for new development, redevelopment, or a mix of new and evelopment?
	New development
	Redevelopment
$\boxtimes$	Mix of New Development and Redevelopment



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

## Checklist (continued)

<b>LID Measures:</b> Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:			
ed.			



#### **Massachusetts Department of Environmental Protection**

Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

Checklist (continued) Standard 2: Peak Rate Attenuation Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding. Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm. Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm. Standard 3: Recharge Soil Analysis provided. Required Recharge Volume calculation provided. Required Recharge volume reduced through use of the LID site Design Credits. Sizing the infiltration, BMPs is based on the following method: Check the method used. ⊠ Static ☐ Simple Dynamic Dynamic Field<sup>1</sup> Runoff from all impervious areas at the site discharging to the infiltration BMP. Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason: Site is comprised solely of C and D soils and/or bedrock at the land surface M.G.L. c. 21E sites pursuant to 310 CMR 40.0000 Solid Waste Landfill pursuant to 310 CMR 19.000 Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable. Calculations showing that the infiltration BMPs will drain in 72 hours are provided. Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

<sup>&</sup>lt;sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

Cr	necklist (continued)
Sta	ndard 3: Recharge (continued)
	The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
	Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.
Sta	ndard 4: Water Quality
The	e Long-Term Pollution Prevention Plan typically includes the following: Good housekeeping practices; Provisions for storing materials and waste products inside or under cover; Vehicle washing controls; Requirements for routine inspections and maintenance of stormwater BMPs; Spill prevention and response plans; Provisions for maintenance of lawns, gardens, and other landscaped areas; Requirements for storage and use of fertilizers, herbicides, and pesticides; Pet waste management provisions; Provisions for operation and management of septic systems; Provisions for solid waste management; Snow disposal and plowing plans relative to Wetland Resource Areas; Winter Road Salt and/or Sand Use and Storage restrictions; Street sweeping schedules; Provisions for prevention of illicit discharges to the stormwater management system; Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL; Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan; List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
	A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.  Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
	is within the Zone II or Interim Wellhead Protection Area
	is near or to other critical areas
	is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
	involves runoff from land uses with higher potential pollutant loads.

☐ The Required Water Quality Volume is reduced through use of the LID site Design Credits.

applicable, the 44% TSS removal pretreatment requirement, are provided.

☐ Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if



## **Massachusetts Department of Environmental Protection**

Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

Checklist (continued) Standard 4: Water Quality (continued) The BMP is sized (and calculations provided) based on: ☐ The ½" or 1" Water Quality Volume or The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume. The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs. A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided. Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs) ☐ The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted *prior* to the discharge of stormwater to the post-construction stormwater BMPs. The NPDES Multi-Sector General Permit does *not* cover the land use. LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan. All exposure has been eliminated. All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list. The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent. Standard 6: Critical Areas The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area. Critical areas and BMPs are identified in the Stormwater Report.



#### **Massachusetts Department of Environmental Protection**

Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

## Checklist (continued)

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:			
	Limited Project		
	Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.  Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area  Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff		
	Bike Path and/or Foot Path		
	Redevelopment Project		
$\boxtimes$	Redevelopment portion of mix of new and redevelopment.		
The implied the and	tain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an planation of why these standards are not met is contained in the Stormwater Report. The project involves redevelopment and a description of all measures that have been taken to prove existing conditions is provided in the Stormwater Report. The redevelopment checklist found folume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment is structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) proves existing conditions.		

#### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

Checklist (continued)

	andard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control ontinued)
	The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has <i>not</i> been included in the Stormwater Report but will be submitted <i>before</i> land disturbance begins.
	The project is <i>not</i> covered by a NPDES Construction General Permit.
	The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the
$\boxtimes$	Stormwater Report.  The project is covered by a NPDES Construction General Permit but no SWPPP been submitted.  The SWPPP will be submitted BEFORE land disturbance begins.
Sta	andard 9: Operation and Maintenance Plan
	The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
	Name of the stormwater management system owners;
	□ Party responsible for operation and maintenance;
	Schedule for implementation of routine and non-routine maintenance tasks;
	☐ Plan showing the location of all stormwater BMPs maintenance access areas;
	☐ Description and delineation of public safety features;
	☐ Operation and Maintenance Log Form.
	The responsible party is <b>not</b> the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
	A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
	A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.
Sta	andard 10: Prohibition of Illicit Discharges
$\boxtimes$	The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
	An Illicit Discharge Compliance Statement is attached;
	NO Illicit Discharge Compliance Statement is attached but will be submitted <i>prior to</i> the discharge of any stormwater to post-construction BMPs.

## APPENDIX B

## GEOTECHNICAL INFORMATION

NRCS Soil Resources Report Test Pit information from Septic System Repair



Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Norfolk and Suffolk Counties, Massachusetts



## **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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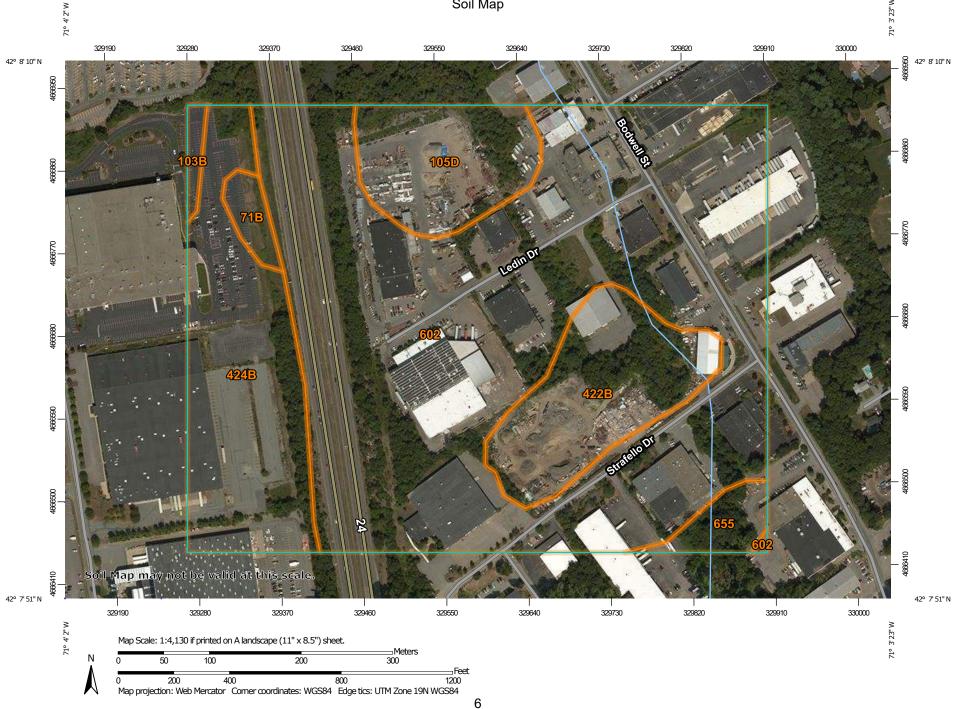
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# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

#### Custom Soil Resource Report Soil Map



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

#### Special Point Features

Blowout (o)

Borrow Pit

Clay Spot

**Closed Depression** 

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

å

Spoil Area Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

#### **Water Features**

Streams and Canals

#### Transportation

---

Rails



Interstate Highways



**US Routes** 



Major Roads



Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 14, Sep 12, 2018

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Aug 26, 2014—Sep 4. 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
71B Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony		1.0	1.2%
103B Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes		0.5	0.6%
105D Rock outcrop-Hollis complex, 3 to 25 percent slopes		5.9	7.6%
422B Canton fine sandy loam, 0 to 8 percent slopes, extremely stony		7.8	10.1%
424B Canton fine sandy loam, 3 to 8 percent slopes, extremely bouldery		12.0	15.7%
602 Urban land, 0 to 15 percent slopes		48.0	62.7%
655 Udorthents, wet substratum		1.5	2.0%
Totals for Area of Interest		76.6	100.0%

## **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas

are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### Norfolk and Suffolk Counties, Massachusetts

#### 71B—Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2w69c

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Ridgebury, extremely stony, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Ridgebury, Extremely Stony**

#### Setting

Landform: Depressions, drumlins, drainageways, hills, ground moraines

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 6 inches: fine sandy loam Bw - 6 to 10 inches: sandy loam

Bg - 10 to 19 inches: gravelly sandy loam Cd - 19 to 66 inches: gravelly sandy loam

#### Properties and qualities

Slope: 3 to 8 percent

Percent of area covered with surface fragments: 9.0 percent Depth to restrictive feature: 15 to 35 inches to densic material

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm) Available water storage in profile: Low (about 3.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D Hydric soil rating: Yes

#### **Minor Components**

#### Woodbridge, extremely stony

Percent of map unit: 10 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Footslope, summit, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Whitman, extremely stony

Percent of map unit: 8 percent Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Paxton, extremely stony

Percent of map unit: 2 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Hydric soil rating: No

#### 103B—Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: vktd

Mean annual precipitation: 32 to 54 inches
Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Charlton and similar soils: 40 percent Hollis and similar soils: 25 percent

Rock outcrop: 20 percent
Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Charlton**

#### Setting

Landform: Hills

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Friable coarse-loamy ablation till derived from granite

#### **Typical profile**

H1 - 0 to 6 inches: fine sandy loam H2 - 6 to 36 inches: fine sandy loam H3 - 36 to 60 inches: fine sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent

Percent of area covered with surface fragments: 1.6 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 7.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A Hydric soil rating: No

#### **Description of Hollis**

#### Setting

Landform: Hills

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Shallow, friable loamy ablation till derived from igneous rock

#### **Typical profile**

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam H3 - 14 to 18 inches: unweathered bedrock

#### **Properties and qualities**

Slope: 3 to 8 percent

Percent of area covered with surface fragments: 1.6 percent Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 1.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D Hydric soil rating: No

#### **Description of Rock Outcrop**

#### Setting

Parent material: Igneous and metamorphic rock

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 0 inches to lithic bedrock

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

#### **Minor Components**

#### Canton

Percent of map unit: 7 percent

Hydric soil rating: No

#### Chatfield

Percent of map unit: 5 percent

Hydric soil rating: No

#### **Scituate**

Percent of map unit: 2 percent

Hydric soil rating: No

#### Whitman

Percent of map unit: 1 percent

Landform: Depressions Hydric soil rating: Yes

#### 105D—Rock outcrop-Hollis complex, 3 to 25 percent slopes

#### **Map Unit Setting**

National map unit symbol: vkxr

Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Rock outcrop: 65 percent

Hollis and similar soils: 25 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Rock Outcrop**

#### Setting

Parent material: Igneous and metamorphic rock

#### **Properties and qualities**

Slope: 15 to 25 percent

Depth to restrictive feature: 0 inches to lithic bedrock

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

#### **Description of Hollis**

#### Setting

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Shallow, friable loamy ablation till

#### Typical profile

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam H3 - 14 to 18 inches: unweathered bedrock

#### **Properties and qualities**

Slope: 3 to 25 percent

Percent of area covered with surface fragments: 9.0 percent Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 1.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D Hydric soil rating: No

#### **Minor Components**

#### Chatfield

Swansea

Percent of map unit: 7 percent Hydric soil rating: No

#### .

Percent of map unit: 2 percent

Landform: Bogs Hydric soil rating: Yes

#### Whitman

Percent of map unit: 1 percent Landform: Depressions Hydric soil rating: Yes

#### 422B—Canton fine sandy loam, 0 to 8 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2w818

Elevation: 0 to 1,180 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Canton, extremely stony, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton, Extremely Stony**

#### Setting

Landform: Ridges, hills, moraines

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

#### Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

#### Properties and qualities

Slope: 0 to 8 percent

Percent of area covered with surface fragments: 9.0 percent

Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water storage in profile: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B Hydric soil rating: No

#### **Minor Components**

#### Charlton, extremely stony

Percent of map unit: 6 percent

Landform: Ground moraines, ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex

Hydric soil rating: No

#### Scituate, extremely stony

Percent of map unit: 6 percent

Landform: Drumlins, ground moraines, hills

Landform position (two-dimensional): Footslope, backslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex

Hydric soil rating: No

#### Montauk, extremely stony

Percent of map unit: 4 percent

Landform: Drumlins, hills, ground moraines, recessionial moraines Landform position (two-dimensional): Backslope, summit, shoulder

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex

Hydric soil rating: No

#### **Swansea**

Percent of map unit: 4 percent

Landform: Depressions, marshes, kettles, swamps, bogs

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 424B—Canton fine sandy loam, 3 to 8 percent slopes, extremely bouldery

#### **Map Unit Setting**

National map unit symbol: vkq5

Elevation: 0 to 1,000 feet

Mean annual precipitation: 45 to 54 inches
Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### Map Unit Composition

Canton and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton**

#### Setting

Landform: Ice-contact slopes

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Friable coarse-loamy eolian deposits over loose sandy and

gravelly ablation till

#### **Typical profile**

H1 - 0 to 3 inches: fine sandy loam
H2 - 3 to 18 inches: fine sandy loam
H3 - 18 to 60 inches: gravelly loamy sand

#### Properties and qualities

Slope: 3 to 8 percent

Percent of area covered with surface fragments: 9.0 percent

Depth to restrictive feature: 18 to 36 inches to strongly contrasting textural

stratification

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: A Hydric soil rating: No

#### **Minor Components**

#### **Montauk**

Percent of map unit: 4 percent Hydric soil rating: No

#### Charlton

Percent of map unit: 2 percent

Hydric soil rating: No

#### Chatfield

Percent of map unit: 2 percent

Hydric soil rating: No

#### **Scituate**

Percent of map unit: 2 percent

Hydric soil rating: No

#### 602—Urban land, 0 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: vkyj

Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F

Frost-free period: 120 to 200 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Urban land: 99 percent
Minor components: 1 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Urban Land**

#### Setting

Parent material: Excavated and filled land

#### **Minor Components**

#### **Rock outcrops**

Percent of map unit: 1 percent Hydric soil rating: Unranked

#### 655—Udorthents, wet substratum

#### **Map Unit Setting**

National map unit symbol: vkyd

Mean annual precipitation: 45 to 54 inches
Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Udorthents and similar soils: 95 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Udorthents**

#### Setting

Landform position (two-dimensional): Shoulder, footslope Landform position (three-dimensional): Riser, tread

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Parent material: Excavated and filled sandy and gravelly human transported

material over highly-decomposed herbaceous organic material

#### Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

#### **Minor Components**

#### **Urban land**

Percent of map unit: 3 percent Hydric soil rating: Unranked

#### **Ipswich**

Percent of map unit: 2 percent

Landform: Marshes Hydric soil rating: Yes

## **Soil Information for All Uses**

## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

#### Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

## **Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

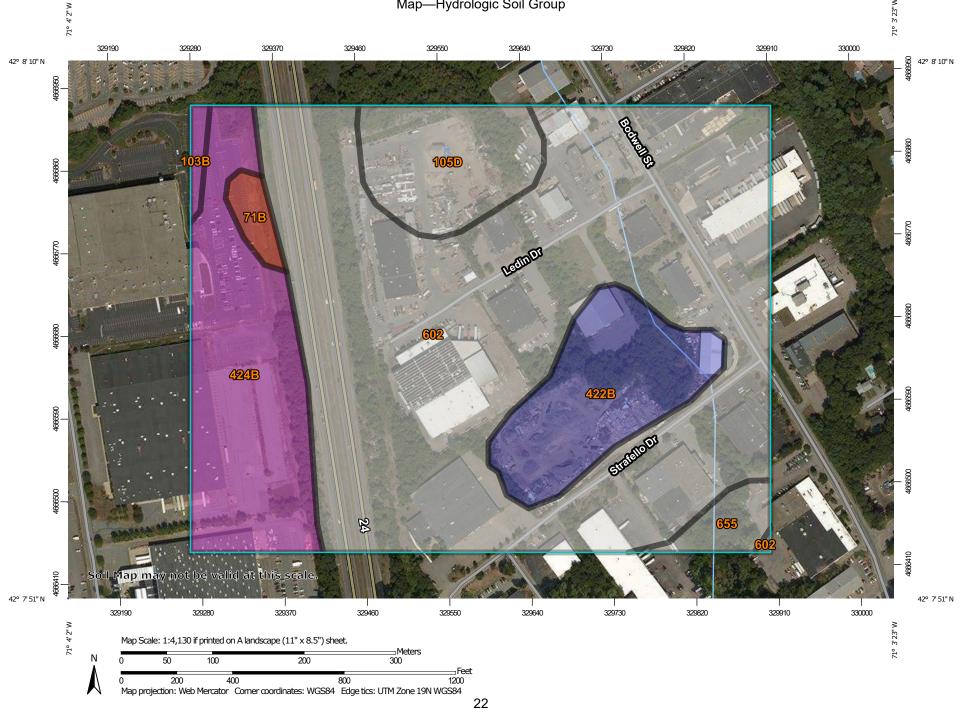
Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Custom Soil Resource Report Map—Hydrologic Soil Group



#### MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at С 1:25.000. Area of Interest (AOI) C/D Soils D Warning: Soil Map may not be valid at this scale. Soil Rating Polygons Not rated or not available Α Enlargement of maps beyond the scale of mapping can cause **Water Features** A/D misunderstanding of the detail of mapping and accuracy of soil Streams and Canals line placement. The maps do not show the small areas of В contrasting soils that could have been shown at a more detailed Transportation scale. B/D Rails ---Interstate Highways Please rely on the bar scale on each map sheet for map C/D **US Routes** measurements. Major Roads Source of Map: Natural Resources Conservation Service Not rated or not available Local Roads Web Soil Survey URL: -Coordinate System: Web Mercator (EPSG:3857) Soil Rating Lines Background Aerial Photography Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Not rated or not available Survey Area Data: Version 14, Sep 12, 2018 **Soil Rating Points** Soil map units are labeled (as space allows) for map scales Α 1:50.000 or larger. A/D Date(s) aerial images were photographed: Aug 26, 2014—Sep 4. 2014 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor

shifting of map unit boundaries may be evident.

## Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
71B	Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony	D	1.0	1.2%
103B	Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes	A	0.5	0.6%
105D	Rock outcrop-Hollis complex, 3 to 25 percent slopes		5.9	7.6%
422B	Canton fine sandy loam, 0 to 8 percent slopes, extremely stony	В	7.8	10.1%
424B	Canton fine sandy loam, 3 to 8 percent slopes, extremely bouldery	A	12.0	15.7%
602	Urban land, 0 to 15 percent slopes		48.0	62.7%
655	Udorthents, wet substratum		1.5	2.0%
Totals for Area of Interest			76.6	100.0%

## Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

# References

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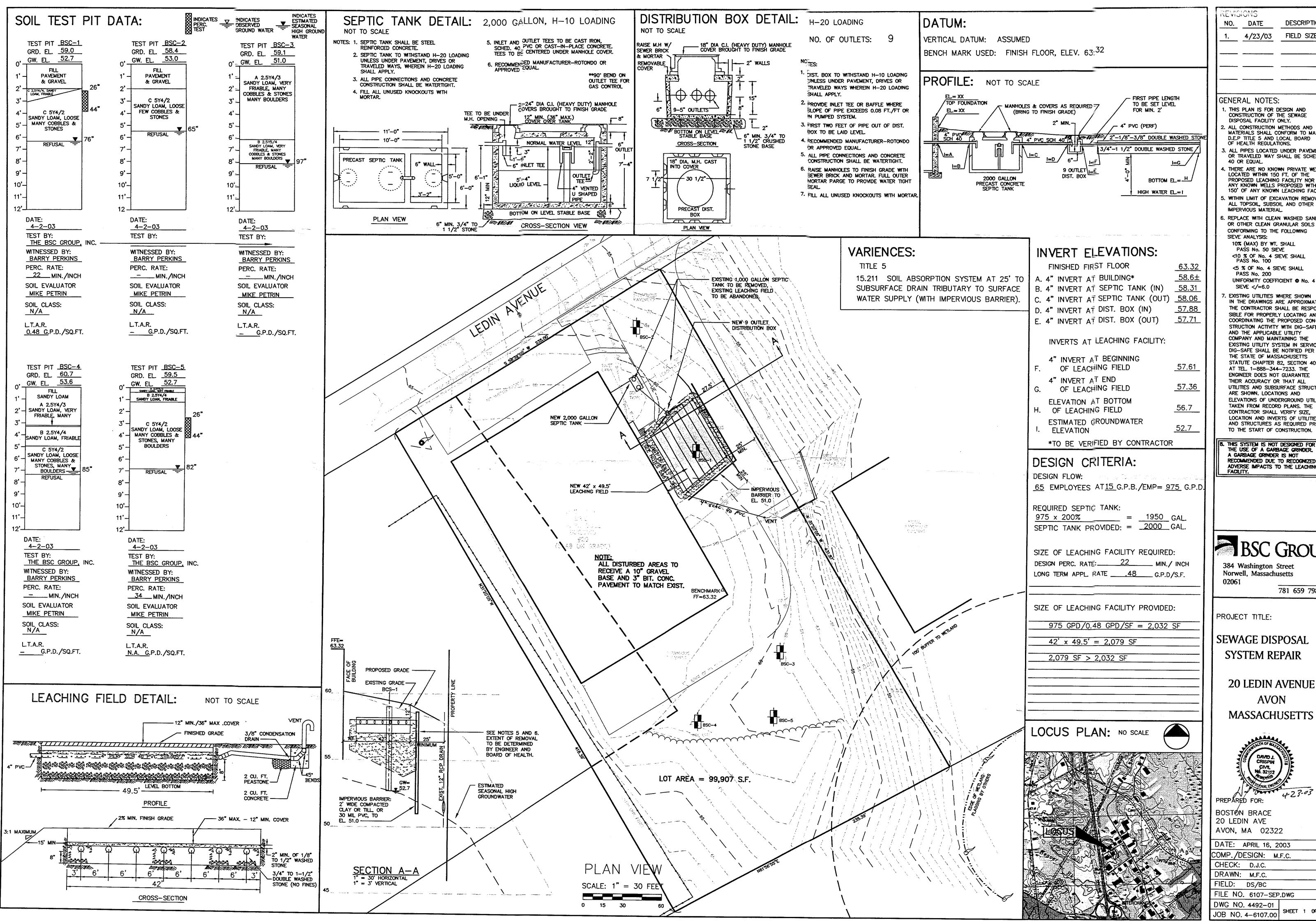
United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/landuse/rangepasture/?cid=stelprdb1043084

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United States Department of Agriculture, Natural Resources Conservation Service. 2006. Land resource regions and major land resource areas of the United States, the Caribbean, and the Pacific Basin. U.S. Department of Agriculture Handbook 296. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2\_053624

United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. http://www.nrcs.usda.gov/Internet/FSE\_DOCUMENTS/nrcs142p2\_052290.pdf



REVISIONS DATE

4/23/03

FIELD SIZE

DESCRIPTION

GENERAL NOTES:

CONSTRUCTION OF THE SEWAGE DISPOSAL FACILITY ONLY. ALL CONSTRUCTION METHODS AND MATERIALS SHALL CONFORM TO MASS. D.E.P TITLE 5 AND LOCAL BOARD OF HEALTH REGULATIONS.

. ALL PIPES LOCATED UNDER PAVEMENT OR TRAVELED WAY SHALL BE SCHEDULE 40 OR EQUAL. THERE ARE NO KNOWN PRIVATE WELLS

LOCATED WITHIN 150 FT. OF THE PROPOSED LEACHING FACILITY NOR ANY KNOWN WELLS PROPOSED WITHIN 150' OF ANY KNOWN LEACHING FACILITY WITHIN LIMIT OF EXCAVATION REMOVE

ALL TOPSOIL, SUBSOIL AND OTHER IMPERVIOUS MATERIAL REPLACE WITH CLEAN WASHED SAND

SIEVE ANALYSIS: 10% (MAX) BY WT. SHALL PASS No. 50 SIEVE <10 % OF No. 4 SIEVE SHALL PASS No. 100

<5 % OF No. 4 SIEVE SHALL PASS No. 200 UNIFORMITY COEFFICIENT O No. 4 SIEVE </=6.0

. EXISTING UTILITIES WHERE SHOWN IN THE DRAWINGS ARE APPROXIMATE THE CONTRACTOR SHALL BE RESPON-SIBLE FOR PROPERLY LOCATING AND COORDINATING THE PROPOSED CON-STRUCTION ACTIVITY WITH DIG-SAFE AND THE APPLICABLE UTILITY COMPANY AND MAINTAINING THE EXISTING UTILITY SYSTEM IN SERVICE. DIG-SAFE SHALL BE NOTIFIED PER THE STATE OF MASSACHUSETTS STATUTE CHAPTER 82, SECTION 409 AT TEL. 1-888-344-7233. THE ENGINEER DOES NOT GUARANTEE THEIR ACCURACY OR THAT ALL UTILITIES AND SUBSURFACE STRUCTURES ARE SHOWN. LOCATIONS AND **ELEVATIONS OF UNDERGROUND UTILITIES** TAKEN FROM RECORD PLANS. THE CONTRACTOR SHALL VERIFY SIZE. LOCATION AND INVERTS OF UTILITIES AND STRUCTURES AS REQUIRED PRIOR TO THE START OF CONSTRUCTION.

B. THIS SYSTEM IS NOT DESIGNED FOR THE USE OF A GARBAGE CRINDER. A GARBAGE GRINDER IS NOT RECOMMENDED DUE TO RECOGNIZED ADVERSE IMPACTS TO THE LEACHING FACILITY.



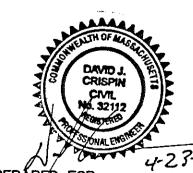
384 Washington Street Norwell, Massachusetts

781 659 7981

PROJECT TITLE:

**SEWAGE DISPOSAL** SYSTEM REPAIR

> 20 LEDIN AVENUE **AVON MASSACHUSETTS**



PREPÁRED FOR:

BOSTÓN BRACE 20 LEDIN AVE AVON, MA 02322

DATE: APRIL 16, 2003 COMP. /DESIGN: M.F.C. CHECK: D.J.C. DRAWN: M.F.C.

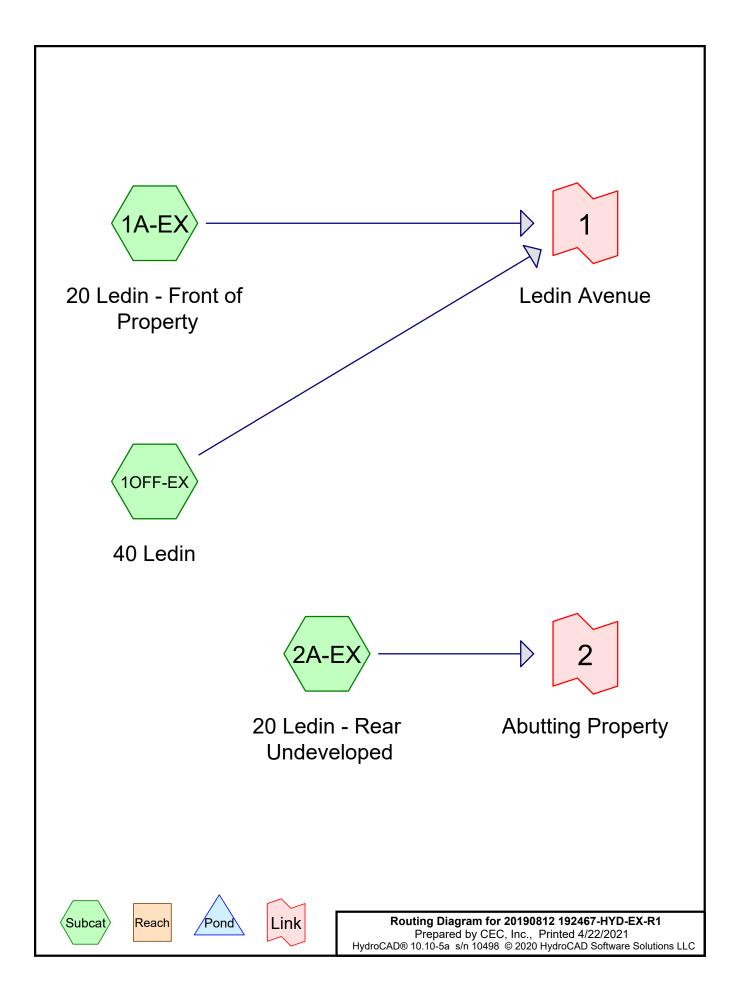
FIELD: DS/BC FILE NO. 6107-SEP.DWG

## **APPENDIX C**

## **SUPPORTING CALCULATIONS**

HydroCAD Drainage Analysis
TSS Removal Calculations
Water Quality Volume and Recharge Calculations
Manufacturer's O&M Procedures





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## Page 2

## **Rainfall Events Listing**

Event#	Event	Storm Type	Curve Mode		Duration	B/B	Depth	AMC
	Name				(hours)		(inches)	
1	2-Year	Type III 24-hr		Default	24.00	1	3.20	2
2	10-Year	Type III 24-hr		Default	24.00	1	4.70	2
3	25-Year	Type III 24-hr		Default	24.00	1	5.50	2
4	100-Year	Type III 24-hr		Default	24.00	1	6.70	2

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## Area Listing (all nodes)

Area	CN	Description	
(acres)		(subcatchment-numbers)	
0.235	69	50-75% Grass cover, Fair, HSG B (1A-EX)	
0.082	79	<50% Grass cover, Poor, HSG B (10FF-EX, 2A-EX)	
0.030	96	Gravel surface, HSG B (1A-EX)	
1.457	98	Paved parking, HSG B (1A-EX, 10FF-EX)	
1.201	98	Roofs, HSG B (1A-EX, 10FF-EX)	
0.775	60	Woods, Fair, HSG B (1A-EX, 2A-EX)	
3.780	88	TOTAL AREA	

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## Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.780	HSG B	1A-EX, 10FF-EX, 2A-EX
0.000	HSG C	
0.000	HSG D	
0.000	Other	
3.780		TOTAL AREA

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## **Ground Covers (all nodes)**

HSG (acre		G-B HS0 res) (acr	G-C HSG- res) (acre			Ground Cover	Subcatchment Numbers
0.0	00 0.	235 0.0	0.00	0.000	0.235	50-75% Grass cover, Fair	1A-EX
0.0	00 0.	082 0.0	0.00	0.000	0.082	<50% Grass cover, Poor	10FF-E
							X, 2A-EX
0.0	00 0.	030 0.0	0.00	0.000	0.030	Gravel surface	1A-EX
0.0	00 1.	457 0.0	0.00	0.000	1.457	Paved parking	1A-EX,
							10FF-E X
0.0	00 1.	201 0.0	0.00	0.000	1.201	Roofs	1A-EX,
							10FF-E
							X
0.0	00 0.	775 0.0	0.00	0.000	0.775	Woods, Fair	1A-EX,
0.0	00 3	.780 0.	000 0.00	0.000	3.780	TOTAL AREA	2A-EX
0.0	<del>00</del> 3	. 7 00 0.	0.00	0.000	3.700	IOIAL AREA	

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## Pipe Listing (all nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)
1	10FF-EX	0.00	0.00	30.0	0.9900	0.025	4.0	4.0	0.0

## Type III 24-hr 2-Year Rainfall=3.20"

#### 20190812 192467-HYD-EX-R1

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-EX: 20 Ledin - Front of Runoff Area=85,204 sf 63.50% Impervious Runoff Depth>1.71"

Flow Length=275' Tc=6.0 min CN=86 Runoff=4.12 cfs 0.279 af

Subcatchment1OFF-EX: 40 Ledin Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>2.69"

Flow Length=656' Tc=6.8 min CN=97 Runoff=4.36 cfs 0.333 af

Subcatchment2A-EX: 20 Ledin - Rear Runoff Area=14,724 sf 0.00% Impervious Runoff Depth>0.39"

Flow Length=255' Slope=0.0900 '/' Tc=6.0 min CN=61 Runoff=0.11 cfs 0.011 af

Link 1: Ledin Avenue Inflow=8.48 cfs 0.612 af

Primary=8.48 cfs 0.612 af

Link 2: Abutting Property Inflow=0.11 cfs 0.011 af

Primary=0.11 cfs 0.011 af

Total Runoff Area = 3.780 ac Runoff Volume = 0.623 af Average Runoff Depth = 1.98" 29.68% Pervious = 1.122 ac 70.32% Impervious = 2.658 ac

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## Summary for Subcatchment 1A-EX: 20 Ledin - Front of Property

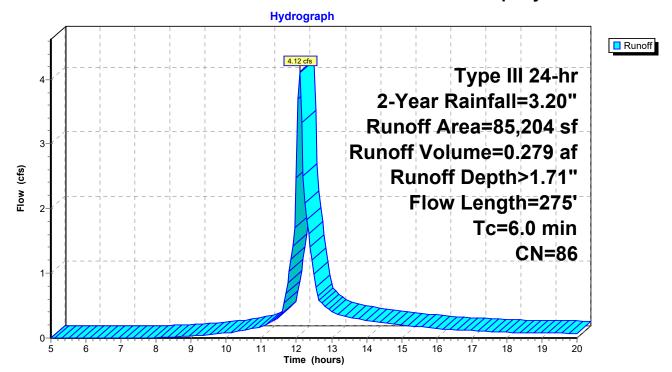
Runoff = 4.12 cfs @ 12.09 hrs, Volume= 0.279 af, Depth> 1.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG B	
		10,237	69	50-75% Gra	ass cover, F	Fair, HSG B
		28,837	98	Paved park	ing, HSG B	
		25,265	98	Roofs, HSC	βB	
		19,558	60	Woods, Fai	r, HSG B	
		85,204	86	Weighted A	verage	
		31,102		36.50% Per	vious Area	
		54,102		63.50% Imp	pervious Are	ea
	Tc	Length	Slope	,	Capacity	Description
_	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	0 4.54		Shallow Concentrated Flow, Front Parking Area and Road
_						Paved Kv= 20.3 fps
	53	275	Total	Increased t	o minimum	Tc = 6.0 min

5.3 275 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1A-EX: 20 Ledin - Front of Property



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## Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 348% of capacity of segment #2

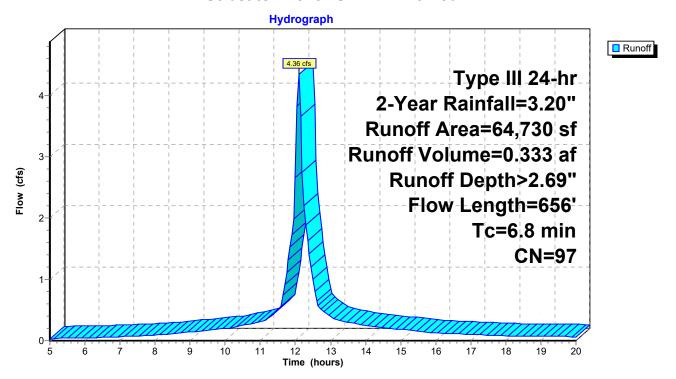
Runoff = 4.36 cfs @ 12.10 hrs, Volume= 0.333 af, Depth> 2.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

_	Α	rea (sf)	CN [	Description		
		27,051	98 F	Roofs, HSC	ВВ	
		3,049	79 <	<50% Gras	s cover, Po	oor, HSG B
_		34,630	98 F	Paved park	ing, HSG E	3
		64,730	97 V	Veighted A	verage	
		3,049	4	I.71% Perv	ious Area	
		61,681	ç	5.29% Imp	ervious Ar	ea
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
						4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
						n= 0.025 Corrugated metal
	0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
						Paved Kv= 20.3 fps
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
						Short Grass Pasture Kv= 7.0 fps
	1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
_						Paved Kv= 20.3 fps
	6.8	656	Total			

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#### Subcatchment 10FF-EX: 40 Ledin



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### Summary for Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped

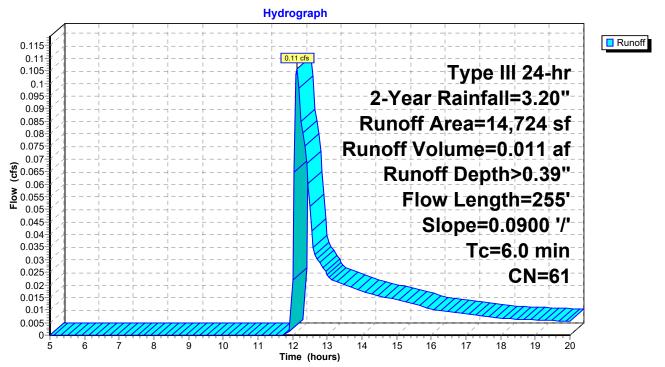
Runoff 0.11 cfs @ 12.13 hrs, Volume= 0.011 af, Depth> 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

	Α	rea (sf)	CN I	Description						
		14,201	60 \	Voods, Fair, HSG B						
		523	79 •	<50% Grass cover, Poor, HSG B						
14,724 61 Weighted Average										
14,724 100.00% Pervious Area						a				
(	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	2.8	255	0.0900	1.50		Shallow Concentrated Flow, Wooded Area				
						Woodland Kv= 5.0 fps				
	2.8	255	Total,	Increased t	o minimum	Tc = 6.0 min				

Total, Increased to minimum Tc = 6.0 min

### Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped



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## **Summary for Link 1: Ledin Avenue**

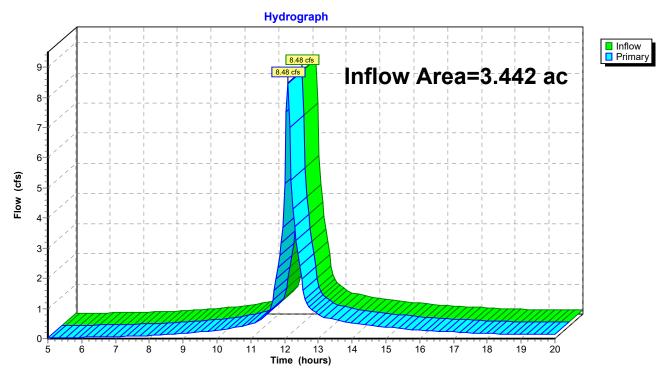
Inflow Area = 3.442 ac, 77.22% Impervious, Inflow Depth > 2.13" for 2-Year event

Inflow = 8.48 cfs @ 12.09 hrs, Volume= 0.612 af

Primary = 8.48 cfs @ 12.09 hrs, Volume= 0.612 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

**Link 1: Ledin Avenue** 



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## **Summary for Link 2: Abutting Property**

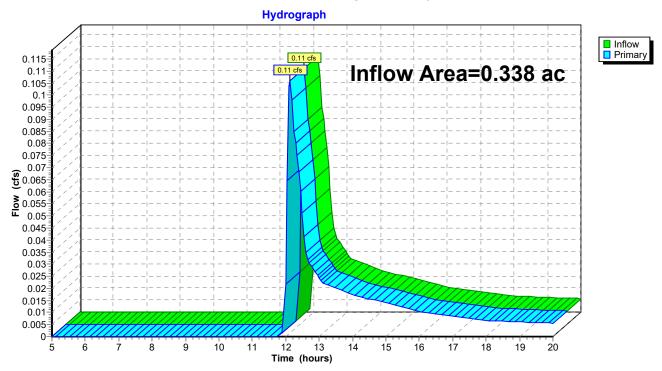
Inflow Area = 0.338 ac, 0.00% Impervious, Inflow Depth > 0.39" for 2-Year event

Inflow = 0.11 cfs @ 12.13 hrs, Volume= 0.011 af

Primary = 0.11 cfs @ 12.13 hrs, Volume= 0.011 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

## **Link 2: Abutting Property**



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Type III 24-hr 10-Year Rainfall=4.70" Printed 4/22/2021

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-EX: 20 Ledin - Front of Runoff Area=85,204 sf 63.50% Impervious Runoff Depth>3.00"

Flow Length=275' Tc=6.0 min CN=86 Runoff=7.08 cfs 0.489 af

Subcatchment1OFF-EX: 40 Ledin Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>4.07"

Flow Length=656' Tc=6.8 min CN=97 Runoff=6.49 cfs 0.503 af

Subcatchment2A-EX: 20 Ledin - Rear Runoff Area=14,724 sf 0.00% Impervious Runoff Depth>1.08"

Flow Length=255' Slope=0.0900 '/' Tc=6.0 min CN=61 Runoff=0.41 cfs 0.030 af

Link 1: Ledin Avenue Inflow=13.56 cfs 0.992 af

Primary=13.56 cfs 0.992 af

Link 2: Abutting Property Inflow=0.41 cfs 0.030 af

Primary=0.41 cfs 0.030 af

Total Runoff Area = 3.780 ac Runoff Volume = 1.022 af Average Runoff Depth = 3.25" 29.68% Pervious = 1.122 ac 70.32% Impervious = 2.658 ac

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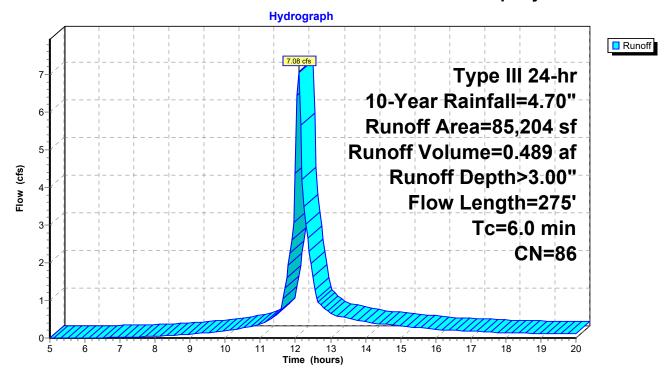
## Summary for Subcatchment 1A-EX: 20 Ledin - Front of Property

Runoff = 7.08 cfs @ 12.09 hrs, Volume= 0.489 af, Depth> 3.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG E	3
		10,237	69	50-75% Gra	ass cover, F	Fair, HSG B
		28,837	98	Paved park	ing, HSG B	3
		25,265	98	Roofs, HSC	βB	
		19,558	60	Woods, Fai	r, HSG B	
		85,204	86	Weighted A	verage	
		31,102		36.50% Per	rvious Area	
		54,102		63.50% Imp	pervious Are	ea
	Тс	Length	Slope	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	3 4.54		Shallow Concentrated Flow, Front Parking Area and Road
_						Paved Kv= 20.3 fps
	5.3	275	Total,	Increased t	o minimum	Tc = 6.0 min

### **Subcatchment 1A-EX: 20 Ledin - Front of Property**



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## Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 518% of capacity of segment #2

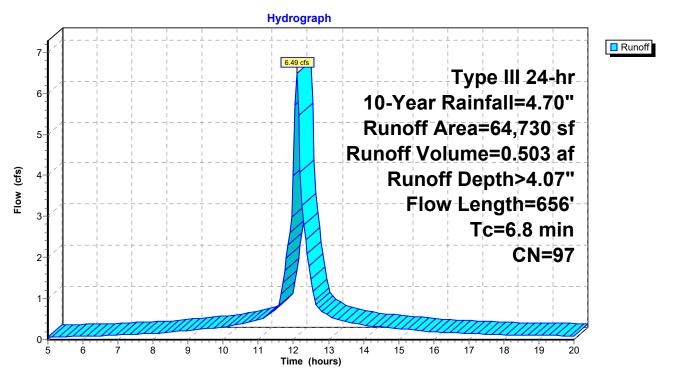
Runoff = 6.49 cfs @ 12.10 hrs, Volume= 0.503 af, Depth> 4.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

	Δ	rea (sf)	CN D	escription		
-	^	27,051		coofs, HSC		
		•				or UCC D
		3,049			•	por, HSG B
_		34,630			ing, HSG E	3
		64,730		Veighted A	•	
		3,049	4	.71% Perv	rious Area	
		61,681	9	5.29% Imp	pervious Ar	ea
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
						4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
						n= 0.025 Corrugated metal
	0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
						Paved Kv= 20.3 fps
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
	0		3.3200	0.00		Short Grass Pasture Kv= 7.0 fps
	1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
	1.0	100	0.0210	3.01		Paved Kv= 20.3 fps
-	6.8	656	Total			1 4704 117 20.0 ipo
	0.0	656	Total			

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### Subcatchment 10FF-EX: 40 Ledin



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### Summary for Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped

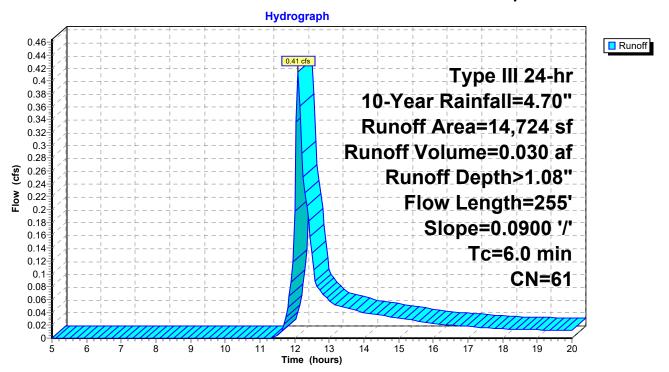
Runoff = 0.41 cfs @ 12.10 hrs, Volume= 0.030 af, Depth> 1.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

 Α	rea (sf)	CN	Description							
	14,201	60	Voods, Fair, HSG B							
	523	79	<50% Gras	50% Grass cover, Poor, HSG B						
	14,724	61	Weighted Average							
	14,724		100.00% P	ervious Are	a					
Tc	Length	Slope	<ul><li>Velocity</li></ul>	Capacity	Description					
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
 2.8	255	0.0900	1.50		Shallow Concentrated Flow, Wooded Area					
					Woodland Kv= 5.0 fps					
20	255	Total	Ingrasad t	a minimum	To = 6.0 min					

2.8 255 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped



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## **Summary for Link 1: Ledin Avenue**

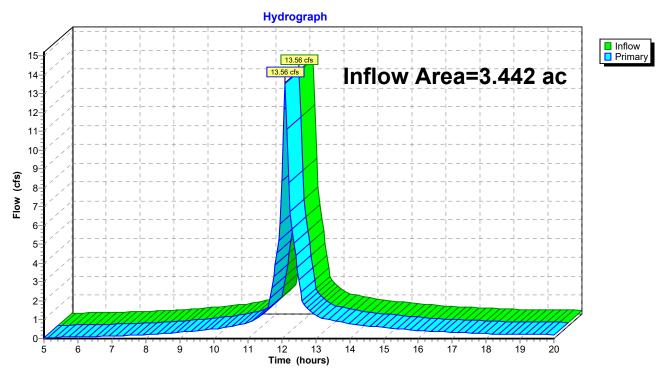
Inflow Area = 3.442 ac, 77.22% Impervious, Inflow Depth > 3.46" for 10-Year event

Inflow = 13.56 cfs @ 12.09 hrs, Volume= 0.992 af

Primary = 13.56 cfs @ 12.09 hrs, Volume= 0.992 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

**Link 1: Ledin Avenue** 



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### **Summary for Link 2: Abutting Property**

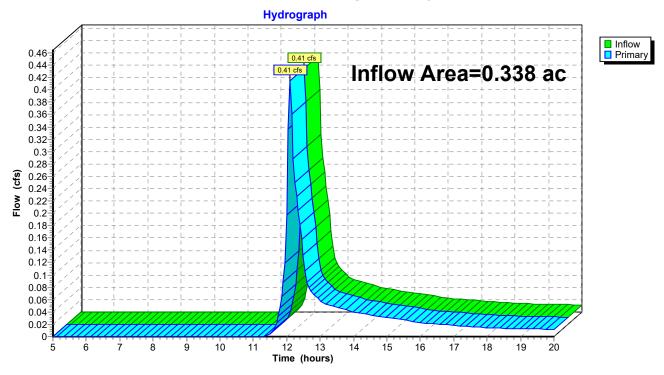
Inflow Area = 0.338 ac, 0.00% Impervious, Inflow Depth > 1.08" for 10-Year event

Inflow = 0.41 cfs @ 12.10 hrs, Volume= 0.030 af

Primary = 0.41 cfs @ 12.10 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

## **Link 2: Abutting Property**



Type III 24-hr 25-Year Rainfall=5.50"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-EX: 20 Ledin - Front of Runoff Area=85,204 sf 63.50% Impervious Runoff Depth>3.71"

Flow Length=275' Tc=6.0 min CN=86 Runoff=8.66 cfs 0.605 af

Subcatchment1OFF-EX: 40 Ledin Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>4.80"

Flow Length=656' Tc=6.8 min CN=97 Runoff=7.63 cfs 0.594 af

Subcatchment2A-EX: 20 Ledin - Rear Runoff Area=14,724 sf 0.00% Impervious Runoff Depth>1.53"

Flow Length=255' Slope=0.0900 '/' Tc=6.0 min CN=61 Runoff=0.61 cfs 0.043 af

Link 1: Ledin Avenue Inflow=16.28 cfs 1.199 af

Primary=16.28 cfs 1.199 af

Link 2: Abutting Property Inflow=0.61 cfs 0.043 af

Primary=0.61 cfs 0.043 af

Total Runoff Area = 3.780 ac Runoff Volume = 1.242 af Average Runoff Depth = 3.94" 29.68% Pervious = 1.122 ac 70.32% Impervious = 2.658 ac

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## Summary for Subcatchment 1A-EX: 20 Ledin - Front of Property

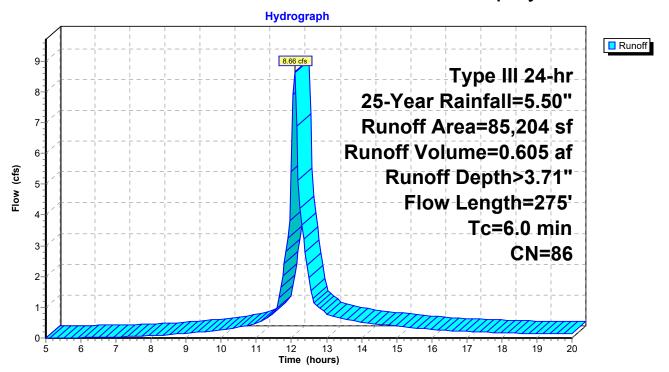
Runoff = 8.66 cfs @ 12.09 hrs, Volume= 0.605 af, Depth> 3.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG B	
		10,237	69	50-75% Gra	ass cover, F	Fair, HSG B
		28,837	98	Paved park	ing, HSG B	
		25,265	98	Roofs, HSC	βB	
		19,558	60	Woods, Fai	r, HSG B	
		85,204	86	Weighted A	verage	
		31,102		36.50% Per	vious Area	
		54,102		63.50% Imp	pervious Are	ea
	Tc	Length	Slope	,	Capacity	Description
_	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	0 4.54		Shallow Concentrated Flow, Front Parking Area and Road
_						Paved Kv= 20.3 fps
	53	275	Total	Increased t	o minimum	Tc = 6.0 min

5.3 275 Total, Increased to minimum Tc = 6.0 min

### **Subcatchment 1A-EX: 20 Ledin - Front of Property**



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## Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 608% of capacity of segment #2

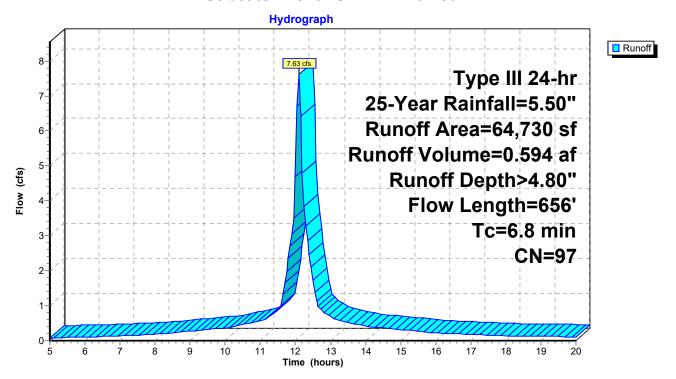
Runoff = 7.63 cfs @ 12.10 hrs, Volume= 0.594 af, Depth> 4.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

	Α	rea (sf)	CN D	<b>Description</b>		
		27,051	98 F	Roofs, HSC	B	
3,049 79 <50% Grass cover, Poor, HSG B						oor, HSG B
34,630 98 Paved parking, HSG B						
64,730 97 Weighted Average						
3,049 4.71% Pervious Area						
61,681 95.29% Impervious Area					ea	
		, -		'		
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
						4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
						n= 0.025 Corrugated metal
	0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
						Paved Kv= 20.3 fps
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
						Short Grass Pasture Kv= 7.0 fps
	1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
_						Paved Kv= 20.3 fps
	6.8	656	Total			

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#### Subcatchment 10FF-EX: 40 Ledin



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### Summary for Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped

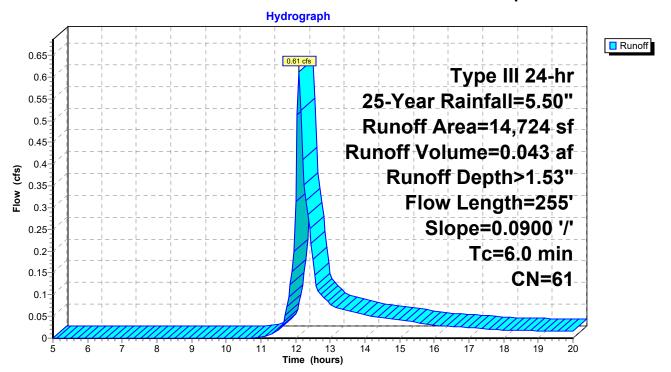
Runoff = 0.61 cfs @ 12.10 hrs, Volume= 0.043 af, Depth> 1.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN	Description					
	14,201	60	Woods, Fair, HSG B					
	523	79	<50% Grass cover, Poor, HSG B					
	14,724 61 Weighted Average							
	14,724 100.00% Pervious Area							
Tc	Length	Slope	<ul> <li>Velocity</li> </ul>	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
2.8	255	0.0900	1.50		Shallow Concentrated Flow, Wooded Area			
					Woodland Kv= 5.0 fps			
20	255	Total	Ingrasad t	o minimuum	To = 6.0 min			

2.8 255 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped



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## **Summary for Link 1: Ledin Avenue**

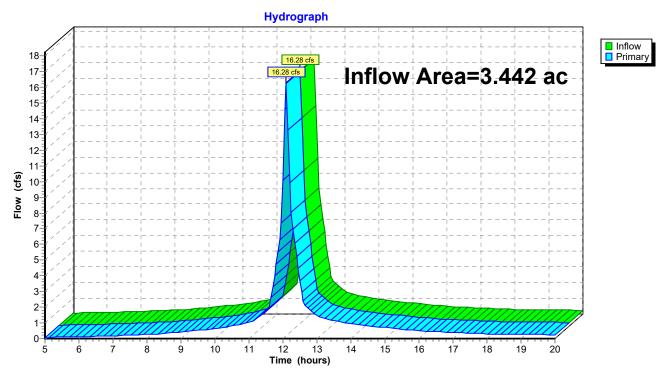
Inflow Area = 3.442 ac, 77.22% Impervious, Inflow Depth > 4.18" for 25-Year event

Inflow = 16.28 cfs @ 12.09 hrs, Volume= 1.199 af

Primary = 16.28 cfs @ 12.09 hrs, Volume= 1.199 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

**Link 1: Ledin Avenue** 



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## **Summary for Link 2: Abutting Property**

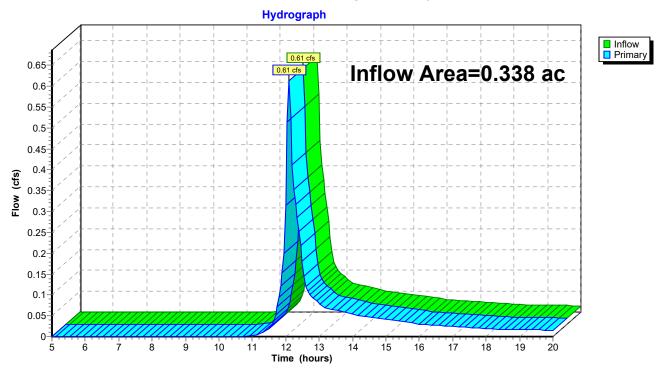
Inflow Area = 0.338 ac, 0.00% Impervious, Inflow Depth > 1.53" for 25-Year event

Inflow = 0.61 cfs @ 12.10 hrs, Volume= 0.043 af

Primary = 0.61 cfs @ 12.10 hrs, Volume= 0.043 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

## **Link 2: Abutting Property**



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Type III 24-hr 100-Year Rainfall=6.70" Printed 4/22/2021

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-EX: 20 Ledin - Front of Runoff Area=85,204 sf 63.50% Impervious Runoff Depth>4.80" Flow Length=275' Tc=6.0 min CN=86 Runoff=11.04 cfs 0.782 af

Subcatchment1OFF-EX: 40 Ledin

Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>5.90"

Flow Length=656' Tc=6.8 min CN=97 Runoff=9.32 cfs 0.730 af

Subcatchment2A-EX: 20 Ledin - Rear Runoff Area=14,724 sf 0.00% Impervious Runoff Depth>2.28" Flow Length=255' Slope=0.0900 '/' Tc=6.0 min CN=61 Runoff=0.94 cfs 0.064 af

**Link 1: Ledin Avenue**Inflow=20.35 cfs 1.512 af

Primary=20.35 cfs 1.512 af

Link 2: Abutting Property

Inflow=0.94 cfs 0.064 af
Primary=0.94 cfs 0.064 af

Total Runoff Area = 3.780 ac Runoff Volume = 1.576 af Average Runoff Depth = 5.00" 29.68% Pervious = 1.122 ac 70.32% Impervious = 2.658 ac

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## Summary for Subcatchment 1A-EX: 20 Ledin - Front of Property

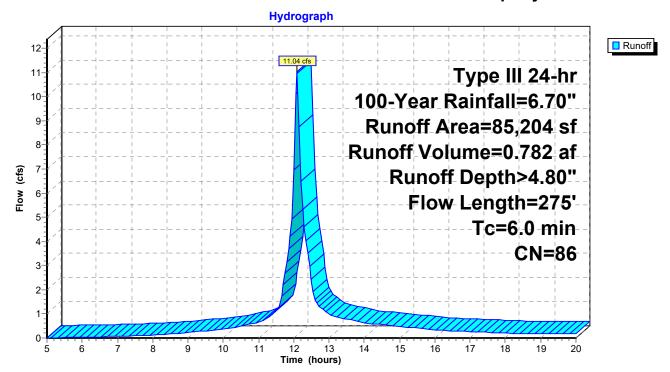
Runoff 11.04 cfs @ 12.09 hrs, Volume= 0.782 af, Depth> 4.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

_	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG B	3
10,237 69 50-75% Grass cover, Fa				50-75% Gra	ass cover, F	Fair, HSG B
28,837 98 Paved parking, HSG B				Paved park	ing, HSG B	
		25,265	98	Roofs, HSC	βΒ	
		19,558	60	Woods, Fai	r, HSG B	
	85,204 86 Weighted Average				verage	<del>-</del>
	31,102 36.50% Pervious Area				rvious Area	
54,102 63.50% Impervious Are					pervious Are	ea
	Tc	Length	Slope	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	3 4.54		Shallow Concentrated Flow, Front Parking Area and Road
						Paved Kv= 20.3 fps
	5.3	275	Total,	Increased t	o minimum	Tc = 6.0 min

Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1A-EX: 20 Ledin - Front of Property



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## Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 743% of capacity of segment #2

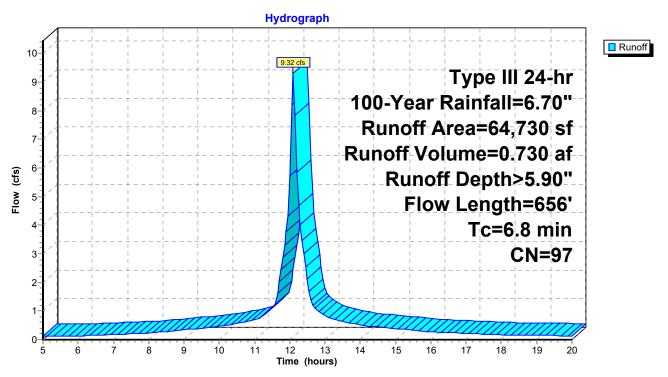
Runoff = 9.32 cfs @ 12.10 hrs, Volume= 0.730 af, Depth> 5.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

	Δ	rea (sf)	CN D	escription		
-	^	27,051				
						or UCC D
3,049 79 <50% Grass cover, Poor, HSG B						
_	34,630 98 Paved parking, HSG B					
64,730 97 Weighted Average						
3,049 4.71% Pervious Area						
	61,681 95.29% Impervious Are					ea
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
						4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
						n= 0.025 Corrugated metal
	0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
						Paved Kv= 20.3 fps
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
	0		3.3200	0.00		Short Grass Pasture Kv= 7.0 fps
	1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
	1.0	100	0.0210	3.01		Paved Kv= 20.3 fps
-	6.8	656	Total			1 4704 117 20.0 ipo
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### Subcatchment 10FF-EX: 40 Ledin



### Summary for Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped

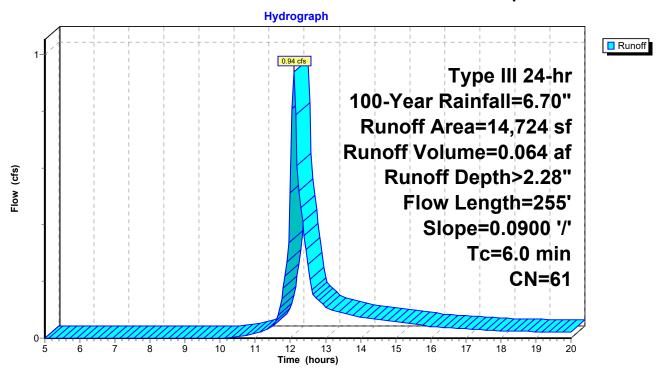
Runoff = 0.94 cfs @ 12.10 hrs, Volume= 0.064 af, Depth> 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

 Α	rea (sf)	CN	Description							
	14,201	60	Woods, Fair, HSG B							
	523	79	<50% Grass cover, Poor, HSG B							
	14,724	61	61 Weighted Average							
	14,724		a							
Тс	Length	Slope	e Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
2.8	255	0.0900	1.50		Shallow Concentrated Flow, Wooded Area					
					Woodland Kv= 5.0 fps					
20	255	Total	Ingragad t	o minimum	To = 6.0 min					

2.8 255 Total, Increased to minimum Tc = 6.0 min

#### Subcatchment 2A-EX: 20 Ledin - Rear Undeveloped



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### **Summary for Link 1: Ledin Avenue**

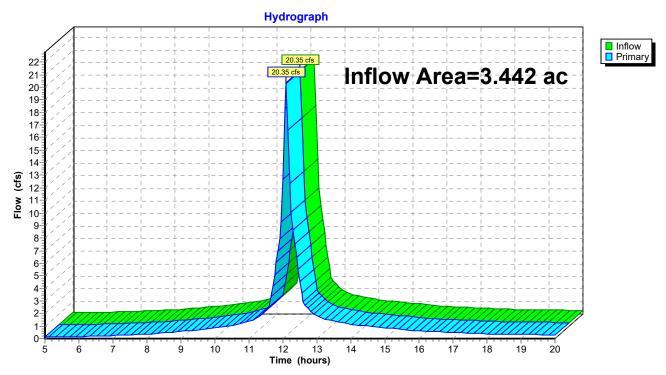
Inflow Area = 3.442 ac, 77.22% Impervious, Inflow Depth > 5.27" for 100-Year event

Inflow = 20.35 cfs @ 12.09 hrs, Volume= 1.512 af

Primary = 20.35 cfs @ 12.09 hrs, Volume= 1.512 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

**Link 1: Ledin Avenue** 



#### 20190812 192467-HYD-EX-R1

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### **Summary for Link 2: Abutting Property**

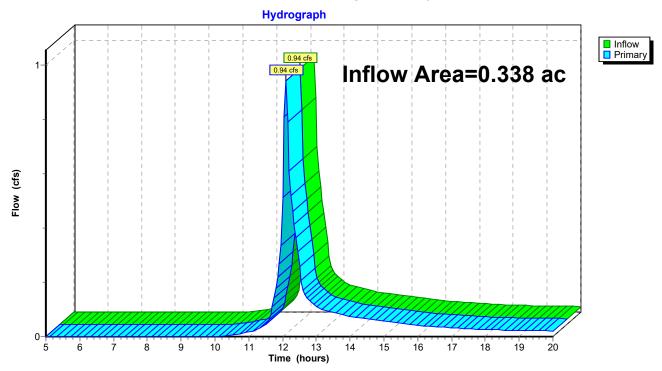
Inflow Area = 0.338 ac, 0.00% Impervious, Inflow Depth > 2.28" for 100-Year event

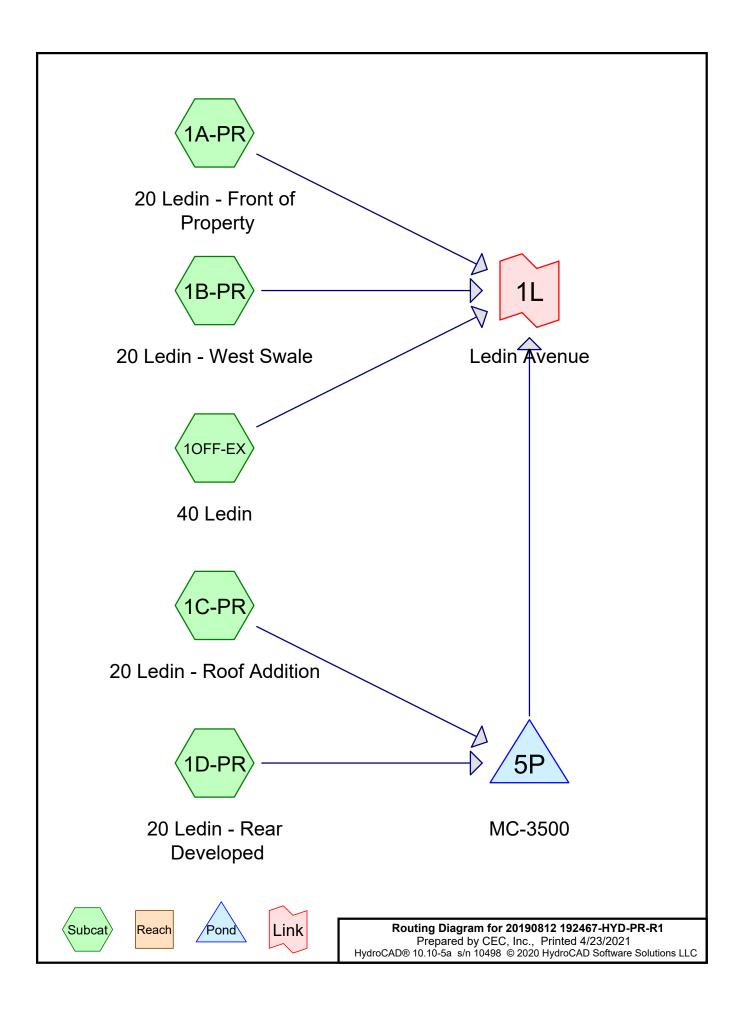
Inflow = 0.94 cfs @ 12.10 hrs, Volume= 0.064 af

Primary = 0.94 cfs @ 12.10 hrs, Volume= 0.064 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

### **Link 2: Abutting Property**





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### **Rainfall Events Listing**

Event#	Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
	Name				(hours)		(inches)	
1	2-Year	Type III 24-hr		Default	24.00	1	3.20	2
2	10-Year	Type III 24-hr		Default	24.00	1	4.70	2
3	25-Year	Type III 24-hr		Default	24.00	1	5.50	2
4	100-Year	Type III 24-hr		Default	24.00	1	6.70	2

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### **Area Listing (all nodes)**

Area	CN	Description
(acres)		(subcatchment-numbers)
0.276	69	50-75% Grass cover, Fair, HSG B (1A-PR, 1B-PR, 1D-PR)
0.070	79	<50% Grass cover, Poor, HSG B (10FF-EX)
0.030	96	Gravel surface, HSG B (1A-PR)
1.809	98	Paved parking, HSG B (1A-PR, 1B-PR, 1D-PR, 1OFF-EX)
1.595	98	Roofs, HSG B (1C-PR, 10FF-EX)
3.780	96	TOTAL AREA

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### Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.780	HSG B	1A-PR, 1B-PR, 1C-PR, 1D-PR, 1OFF-EX
0.000	HSG C	
0.000	HSG D	
0.000	Other	
3.780		TOTAL AREA

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### **Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.276	0.000	0.000	0.000	0.276	50-75% Grass cover, Fair	1A-PR, 1B-PR,
0.000	0.070	0.000	0.000	0.000	0.070	<50% Grass cover, Poor	1D-PR 1OFF-E X
0.000 0.000	0.030 1.809	0.000 0.000	0.000 0.000	0.000 0.000	0.030 1.809	Gravel surface Paved parking	1A-PR 1A-PR,
							1B-PR, 1D-PR, 10FF-E
0.000	1.595	0.000	0.000	0.000	1.595	Roofs	X 1C-PR,
							10FF-E X
0.000	3.780	0.000	0.000	0.000	3.780	TOTAL AREA	

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### Pipe Listing (all nodes)

	Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill
_		Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)
	1	1C-PR	0.00	0.00	40.0	0.9900	0.010	0.0	8.0	0.0
	2	1C-PR	0.00	0.00	43.0	0.0250	0.010	0.0	12.0	0.0
	3	10FF-EX	0.00	0.00	30.0	0.9900	0.025	4.0	4.0	0.0
	4	5P	235.00	234.90	5.0	0.0200	0.012	0.0	12.0	0.0

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-PR: 20 Ledin - Front of Runoff Area=26,398 sf 79.87% Impervious Runoff Depth>2.44"

Flow Length=275' Tc=6.0 min CN=93 Runoff=1.64 cfs 0.123 af

Subcatchment1B-PR: 20 Ledin - West Runoff Area=9,191 sf 25.59% Impervious Runoff Depth>1.15"

Flow Length=151' Slope=0.0200 '/' Tc=6.0 min CN=76 Runoff=0.27 cfs 0.020 af

**Subcatchment1C-PR: 20 Ledin - Roof** Runoff Area=42,427 sf 100.00% Impervious Runoff Depth>2.97"

Flow Length=279' Tc=6.0 min CN=98 Runoff=2.95 cfs 0.241 af

Subcatchment1D-PR: 20 Ledin - Rear Runoff Area=21,919 sf 94.62% Impervious Runoff Depth>2.75"

Flow Length=273' Tc=6.0 min CN=96 Runoff=1.47 cfs 0.115 af

Subcatchment1OFF-EX: 40 Ledin Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>2.85"

Flow Length=656' Tc=6.8 min CN=97 Runoff=4.36 cfs 0.353 af

**Pond 5P: MC-3500** Peak Elev=238.43' Storage=5,715 cf Inflow=4.43 cfs 0.356 af

Discarded=0.07 cfs 0.105 af Primary=1.82 cfs 0.207 af Outflow=1.88 cfs 0.312 af

Link 1L: Ledin Avenue Inflow=7.54 cfs 0.704 af

Primary=7.54 cfs 0.704 af

Total Runoff Area = 3.780 ac Runoff Volume = 0.853 af Average Runoff Depth = 2.71" 9.95% Pervious = 0.376 ac 90.05% Impervious = 3.404 ac

### Summary for Subcatchment 1A-PR: 20 Ledin - Front of Property

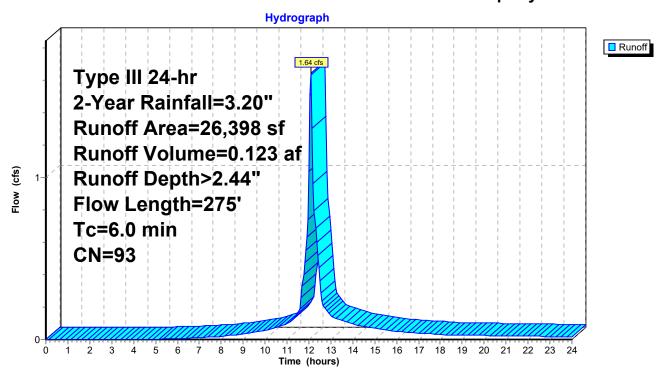
Runoff = 1.64 cfs @ 12.09 hrs, Volume= 0.123 af, Depth> 2.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

_	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG E	3
		4,008	69	50-75% Gra	ass cover, F	Fair, HSG B
		21,083	98	Paved park	ing, HSG B	
		26,398	93	Weighted A	verage	
		5,315		20.13% Per	rvious Area	
		21,083		79.87% Imp	pervious Ar	ea
	Tc	Length	Slope	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	0 4.54		Shallow Concentrated Flow, Front Parking Area and Road
						Paved Kv= 20.3 fps
	5.3	275	Total,	Increased t	o minimum	Tc = 6.0 min

270 Total, morodoca to minimum To 0.0 min

### Subcatchment 1A-PR: 20 Ledin - Front of Property



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### Summary for Subcatchment 1B-PR: 20 Ledin - West Swale

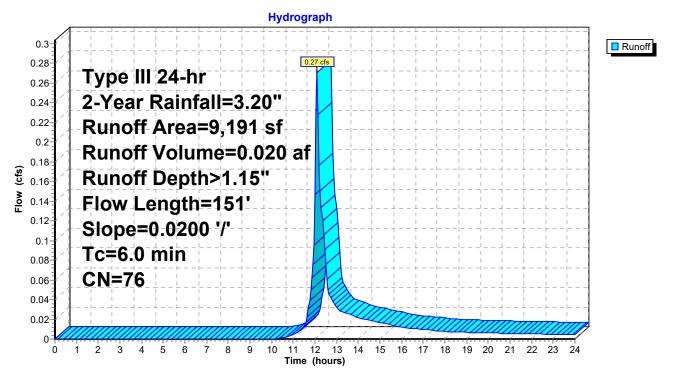
Runoff = 0.27 cfs @ 12.10 hrs, Volume= 0.020 af, Depth> 1.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

_	Α	rea (sf)	CN	I Description						
		6,839	69	50-75% Gra	ass cover, f	Fair, HSG B				
_		2,352	98	Paved parking, HSG B						
		9,191	76	Weighted A	verage					
		6,839	•	74.41% Pervious Area						
		2,352	:	25.59% Impervious Area						
	_				_					
	Tc	Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass				
_						Short Grass Pasture Kv= 7.0 fps				
	2.5	151	Tatal	1		To - 6.0 min				

2.5 151 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1B-PR: 20 Ledin - West Swale



### Summary for Subcatchment 1C-PR: 20 Ledin - Roof Addition

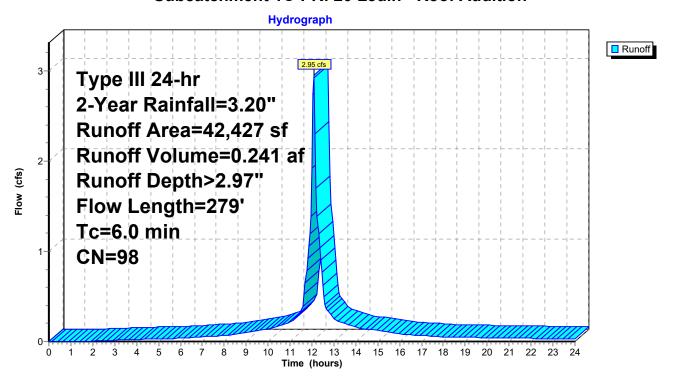
Runoff = 2.95 cfs @ 12.09 hrs, Volume= 0.241 af, Depth> 2.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

A	rea (sf)	CN D	escription				
	24,132	98 F	oofs, HSC	ВВ			
	18,295	98 F	Roofs, HSC	6 B			
	42,427	98 V	Veighted A	verage			
	42,427	1	00.00% In	npervious A	Area		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
2.7	196	0.0100	1.19		Sheet Flow,		
					Smooth surfaces n= 0.011 P2= 3.20"		
0.0	40	0.9900	44.78	15.63	Pipe Channel, Gutter		
					8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'		
					n= 0.010 PVC, smooth interior		
0.1	43	0.0250	9.32	7.32	Pipe Channel,		
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
					n= 0.010 PVC, smooth interior		
- 0 0	070	<del> </del>	1.4		To a Committee		

2.8 279 Total, Increased to minimum Tc = 6.0 min

#### Subcatchment 1C-PR: 20 Ledin - Roof Addition



### Summary for Subcatchment 1D-PR: 20 Ledin - Rear Developed

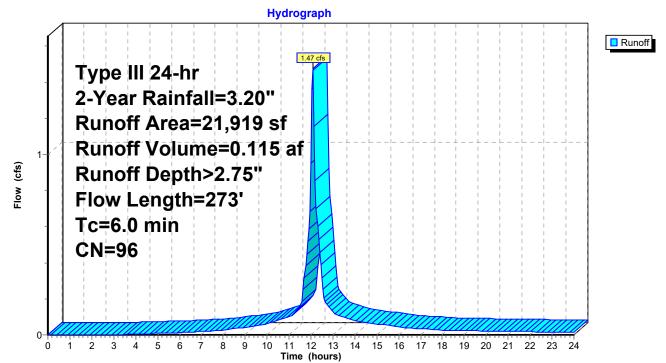
Runoff = 1.47 cfs @ 12.09 hrs, Volume= 0.115 af, Depth> 2.75"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

_	Α	rea (sf)	CN E	escription						
		1,179	69 5	69 50-75% Grass cover, Fair, HSG B						
		20,740	98 F	Paved park	ing, HSG E	3				
		21,919	96 V	96 Weighted Average						
		1,179	5	.38% Perv	ious Area					
		20,740	9	4.62% Imp	pervious Ar	ea				
	_					<b>–</b>				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass				
						Short Grass Pasture Kv= 7.0 fps				
	0.4	74	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot				
						Paved Kv= 20.3 fps				
	8.0	48	0.0200	0.99		Shallow Concentrated Flow, 20 Ledin Grassed Area				
_						Short Grass Pasture Kv= 7.0 fps				
	3.7	273	Total I	nergaead t	o minimum	To = 6.0 min				

3.7 273 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1D-PR: 20 Ledin - Rear Developed



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### Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 348% of capacity of segment #2

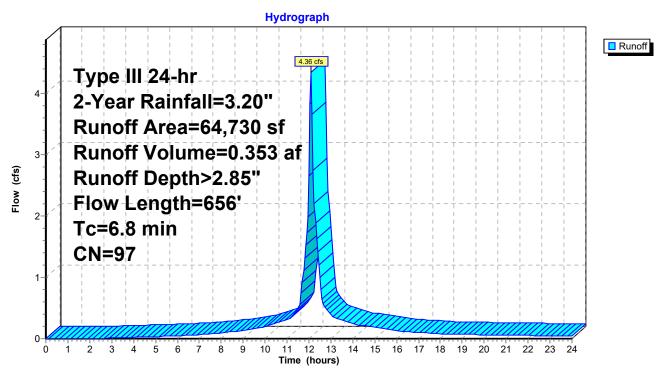
Runoff = 4.36 cfs @ 12.10 hrs, Volume= 0.353 af, Depth> 2.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

 Α	rea (sf)	CN E	Description		
	27,051	98 F	Roofs, HSC	B	
	3,049	79 <	50% Gras	s cover, Po	oor, HSG B
	34,630	98 F	Paved park	ing, HSG E	3
	64,730	97 V	Veighted A	verage	
	3,049		.71% Perv	•	
	61,681	g	5.29% Imp	pervious Ar	ea
	•		•		
Tc	Length	Slope	Velocity	Capacity	Description
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
					Smooth surfaces n= 0.011 P2= 3.20"
0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
					4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
					n= 0.025 Corrugated metal
0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
					Paved Kv= 20.3 fps
2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
					Short Grass Pasture Kv= 7.0 fps
1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
					Paved Kv= 20.3 fps
6.8	656	Total			

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### Subcatchment 10FF-EX: 40 Ledin



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### **Summary for Pond 5P: MC-3500**

Inflow Area = 1.477 ac, 98.17% Impervious, Inflow Depth > 2.89" for 2-Year event Inflow 4.43 cfs @ 12.09 hrs, Volume= 0.356 af 1.88 cfs @ 12.29 hrs, Volume= Outflow 0.312 af, Atten= 57%, Lag= 12.0 min Discarded = 0.07 cfs @ 7.15 hrs, Volume= 0.105 af Primary = 1.82 cfs @ 12.29 hrs, Volume= 0.207 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 238.43' @ 12.29 hrs Surf.Area= 2,790 sf Storage= 5,715 cf

Plug-Flow detention time= 124.6 min calculated for 0.311 af (87% of inflow) Center-of-Mass det. time= 68.6 min ( 830.3 - 761.7 )

Volume	Invert	Avail.Storage	Storage Description
#1A	235.50'	3,956 cf	44.25'W x 63.06'L x 5.50'H Field A
			15,347 cf Overall - 5,456 cf Embedded = 9,891 cf x 40.0% Voids
#2A	236.25'	5,456 cf	ADS_StormTech MC-3500 d +Capx 48 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			48 Chambers in 6 Rows
			Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf
		9,413 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	235.00'	<b>12.0" Round Culvert</b> L= 5.0' Ke= 1.000
	•		Inlet / Outlet Invert= 235.00' / 234.90' S= 0.0200 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf
#2	Device 1	239.00'	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	236.75'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	237.50'	<b>8.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#5	Discarded	235.50'	1.020 in/hr Exfiltration over Surface area

**Discarded OutFlow** Max=0.07 cfs @ 7.15 hrs HW=235.56' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=1.82 cfs @ 12.29 hrs HW=238.43' (Free Discharge)

-1=Culvert (Passes 1.82 cfs of 4.86 cfs potential flow)

-2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

**—3=Orifice/Grate** (Orifice Controls 0.52 cfs @ 5.92 fps)

4=Orifice/Grate (Orifice Controls 1.30 cfs @ 3.72 fps)

#### Pond 5P: MC-3500 - Chamber Wizard Field A

# Chamber Model = ADS\_StormTechMC-3500 d +Cap (ADS StormTech® MC-3500 d rev 03/14 with Cap volume)

Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf

77.0" Wide + 9.0" Spacing = 86.0" C-C Row Spacing

8 Chambers/Row x 7.17' Long +1.85' Cap Length x 2 = 61.06' Row Length +12.0" End Stone x 2 = 63.06' Base Length

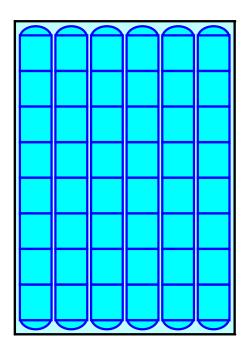
6 Rows x 77.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.25' Base Width 9.0" Stone Base + 45.0" Chamber Height + 12.0" Stone Cover = 5.50' Field Height

48 Chambers x 110.0 cf + 14.9 cf Cap Volume x 2 x 6 Rows = 5,456.5 cf Chamber Storage

15,347.2 cf Field - 5,456.5 cf Chambers = 9,890.7 cf Stone x 40.0% Voids = 3,956.3 cf Stone Storage

Chamber Storage + Stone Storage = 9,412.8 cf = 0.216 af Overall Storage Efficiency = 61.3% Overall System Size = 63.06' x 44.25' x 5.50'

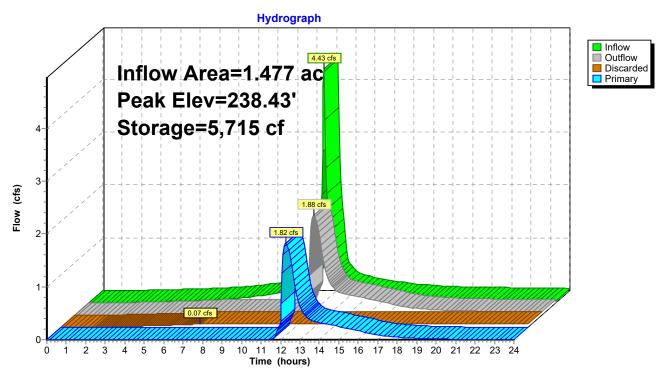
48 Chambers 568.4 cy Field 366.3 cy Stone





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#### Pond 5P: MC-3500



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## Summary for Link 1L: Ledin Avenue

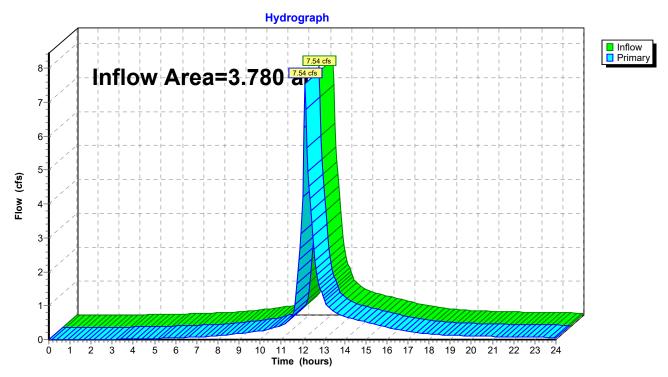
Inflow Area = 3.780 ac, 90.05% Impervious, Inflow Depth > 2.24" for 2-Year event

Inflow = 7.54 cfs @ 12.11 hrs, Volume= 0.704 af

Primary = 7.54 cfs @ 12.11 hrs, Volume= 0.704 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### **Link 1L: Ledin Avenue**



### Type III 24-hr 10-Year Rainfall=4.70"

#### 20190812 192467-HYD-PR-R1

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-PR: 20 Ledin - Front of Runoff Area=26,398 sf 79.87% Impervious Runoff Depth>3.90"

Flow Length=275' Tc=6.0 min CN=93 Runoff=2.56 cfs 0.197 af

Subcatchment1B-PR: 20 Ledin - West Runoff Area=9,191 sf 25.59% Impervious Runoff Depth>2.29"

Flow Length=151' Slope=0.0200 '/' Tc=6.0 min CN=76 Runoff=0.55 cfs 0.040 af

Subcatchment1C-PR: 20 Ledin - Roof Runoff Area=42,427 sf 100.00% Impervious Runoff Depth>4.46"

Flow Length=279' Tc=6.0 min CN=98 Runoff=4.37 cfs 0.362 af

Subcatchment1D-PR: 20 Ledin - Rear Runoff Area=21,919 sf 94.62% Impervious Runoff Depth>4.23"

Flow Length=273' Tc=6.0 min CN=96 Runoff=2.22 cfs 0.177 af

Subcatchment1OFF-EX: 40 Ledin Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>4.34"

Flow Length=656' Tc=6.8 min CN=97 Runoff=6.49 cfs 0.538 af

**Pond 5P: MC-3500** Peak Elev=239.27' Storage=7,283 cf Inflow=6.59 cfs 0.540 af

Discarded=0.07 cfs 0.114 af Primary=4.23 cfs 0.377 af Outflow=4.30 cfs 0.490 af

Link 1L: Ledin Avenue Inflow=12.09 cfs 1.152 af

Primary=12.09 cfs 1.152 af

Total Runoff Area = 3.780 ac Runoff Volume = 1.315 af Average Runoff Depth = 4.17" 9.95% Pervious = 0.376 ac 90.05% Impervious = 3.404 ac

### Summary for Subcatchment 1A-PR: 20 Ledin - Front of Property

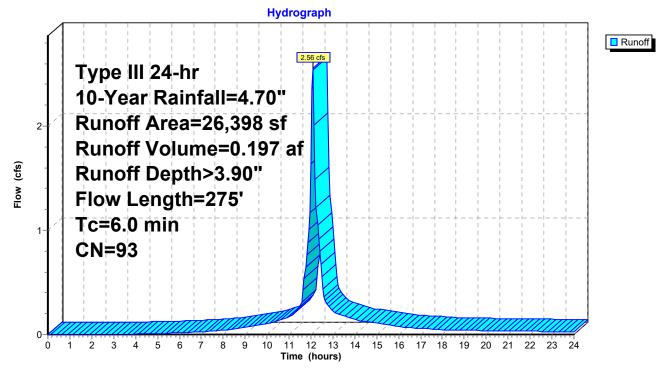
Runoff 2.56 cfs @ 12.09 hrs, Volume= 0.197 af, Depth> 3.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

_	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG B	
		4,008	69	50-75% Gra	ass cover, F	Fair, HSG B
		21,083	98	Paved park	ing, HSG B	
		26,398	93	Weighted A	verage	
		5,315		20.13% Per	vious Area	
		21,083		79.87% Imp	ervious Are	ea
	Тс	Length	Slope	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	4.54		Shallow Concentrated Flow, Front Parking Area and Road
_						Paved Kv= 20.3 fps
	5.3	275	Total,	Increased t	o minimum	Tc = 6.0 min

275 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1A-PR: 20 Ledin - Front of Property

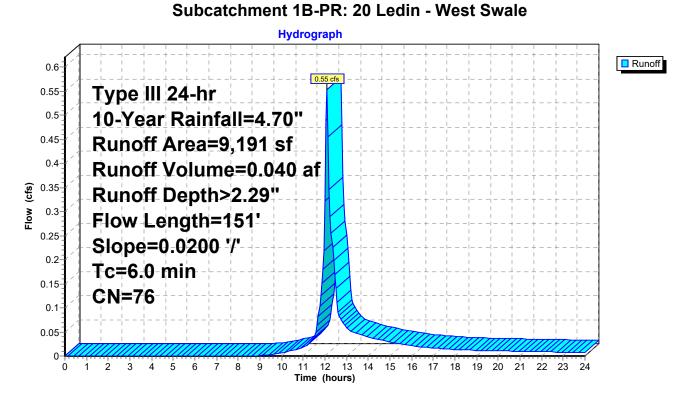


### Summary for Subcatchment 1B-PR: 20 Ledin - West Swale

Runoff = 0.55 cfs @ 12.09 hrs, Volume= 0.040 af, Depth> 2.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN [	Description								
	6,839	69 5	50-75% Grass cover, Fair, HSG B								
	2,352	98 F	Paved park	ing, HSG B	3						
	9,191	76 \	Weighted Average								
	6,839	7	74.41% Per	vious Area							
	2,352	2	25.59% lmp	pervious Ar	ea						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description						
2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass						
					Short Grass Pasture Kv= 7.0 fps						
2.5	151	Total,	Increased t	o minimum	Tc = 6.0 min						



### Summary for Subcatchment 1C-PR: 20 Ledin - Roof Addition

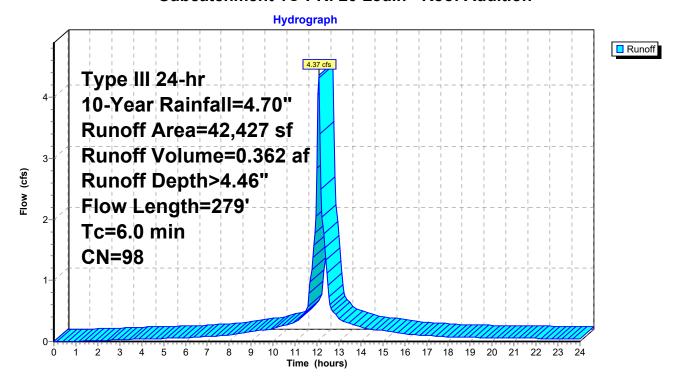
Runoff = 4.37 cfs @ 12.09 hrs, Volume= 0.362 af, Depth> 4.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN D	escription		
	24,132	98 F	oofs, HSC	ВВ	
	18,295	98 F	Roofs, HSC	6 B	
	42,427	98 V	Veighted A	verage	
	42,427	1	00.00% In	npervious A	Area
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.7	196	0.0100	1.19		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.20"
0.0	40	0.9900	44.78	15.63	Pipe Channel, Gutter
					8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'
					n= 0.010 PVC, smooth interior
0.1	43	0.0250	9.32	7.32	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.010 PVC, smooth interior
- 0 0	070	<del> </del>	1.4		To a Committee

2.8 279 Total, Increased to minimum Tc = 6.0 min

#### Subcatchment 1C-PR: 20 Ledin - Roof Addition



### Summary for Subcatchment 1D-PR: 20 Ledin - Rear Developed

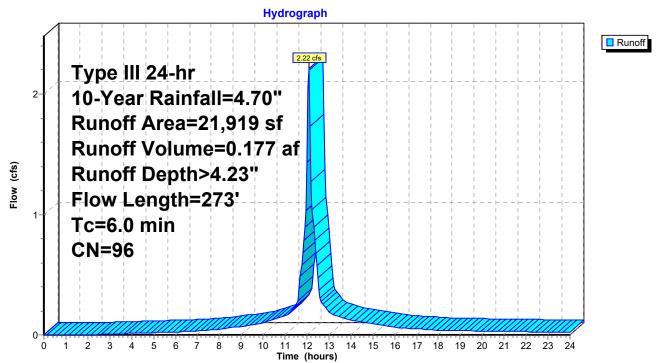
Runoff = 2.22 cfs @ 12.09 hrs, Volume= 0.177 af, Depth> 4.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

_	Α	rea (sf)	CN E	escription						
		1,179	69 5	50-75% Grass cover, Fair, HSG B						
_		20,740	98 F	aved park	ing, HSG B	3				
		21,919	96 V	Veighted A	verage					
		1,179	5	.38% Perv	ious Area					
		20,740	9	4.62% Imp	pervious Ar	ea				
	_									
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass				
						Short Grass Pasture Kv= 7.0 fps				
	0.4	74	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot				
						Paved Kv= 20.3 fps				
	8.0	48	0.0200	0.99		Shallow Concentrated Flow, 20 Ledin Grassed Area				
_						Short Grass Pasture Kv= 7.0 fps				
	37	272	Total I	neraced t	o minimum	Tc = 6.0 min				

3.7 273 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1D-PR: 20 Ledin - Rear Developed



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### Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 518% of capacity of segment #2

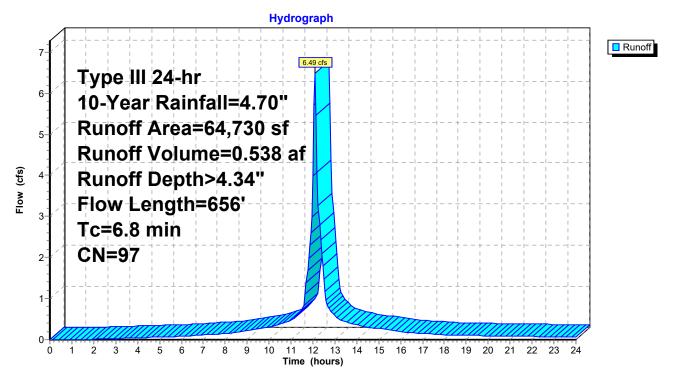
Runoff = 6.49 cfs @ 12.10 hrs, Volume= 0.538 af, Depth> 4.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

	Α	rea (sf)	CN D	escription		
27,051 98 Roofs, HSG B						
		3,049	79 <	50% Gras	s cover, Po	oor, HSG B
		34,630	98 P	aved park	ing, HSG E	3
-		64,730	97 V	Veighted A	verage	
		3,049		.71% Perv	•	
		61,681	9	5.29% Imr	ervious Ar	ea
		, -		'		
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
						4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
						n= 0.025 Corrugated metal
	0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
						Paved Kv= 20.3 fps
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
						Short Grass Pasture Kv= 7.0 fps
	1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
						Paved Kv= 20.3 fps
	6.8	656	Total	•		

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#### Subcatchment 10FF-EX: 40 Ledin



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### **Summary for Pond 5P: MC-3500**

Inflow Area = 1.477 ac, 98.17% Impervious, Inflow Depth > 4.38" for 10-Year event Inflow 6.59 cfs @ 12.09 hrs, Volume= 0.540 af 4.30 cfs @ 12.19 hrs, Volume= Outflow 0.490 af, Atten= 35%, Lag= 6.4 min Discarded = 0.07 cfs @ 5.15 hrs, Volume= 0.114 af 4.23 cfs @ 12.19 hrs, Volume= Primary = 0.377 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 239.27' @ 12.19 hrs Surf.Area= 2,790 sf Storage= 7,283 cf

Plug-Flow detention time= 104.4 min calculated for 0.489 af (91% of inflow) Center-of-Mass det. time= 58.7 min (812.2 - 753.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	235.50'	3,956 cf	44.25'W x 63.06'L x 5.50'H Field A
			15,347 cf Overall - 5,456 cf Embedded = 9,891 cf x 40.0% Voids
#2A	236.25'	5,456 cf	ADS_StormTech MC-3500 d +Capx 48 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			48 Chambers in 6 Rows
			Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf
		9,413 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	235.00'	<b>12.0" Round Culvert</b> L= 5.0' Ke= 1.000
	•		Inlet / Outlet Invert= 235.00' / 234.90' S= 0.0200 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf
#2	Device 1	239.00'	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	236.75'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	237.50'	<b>8.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#5	Discarded	235.50'	1.020 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.07 cfs @ 5.15 hrs HW=235.56' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=4.18 cfs @ 12.19 hrs HW=239.26' (Free Discharge)

**-1=Culvert** (Passes 4.18 cfs of 5.50 cfs potential flow)

2=Broad-Crested Rectangular Weir (Weir Controls 1.52 cfs @ 1.45 fps)

**—3=Orifice/Grate** (Orifice Controls 0.64 cfs @ 7.37 fps)

4=Orifice/Grate (Orifice Controls 2.01 cfs @ 5.76 fps)

#### Pond 5P: MC-3500 - Chamber Wizard Field A

# Chamber Model = ADS\_StormTechMC-3500 d +Cap (ADS StormTech® MC-3500 d rev 03/14 with Cap volume)

Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf

77.0" Wide + 9.0" Spacing = 86.0" C-C Row Spacing

8 Chambers/Row x 7.17' Long +1.85' Cap Length x 2 = 61.06' Row Length +12.0" End Stone x 2 = 63.06' Base Length

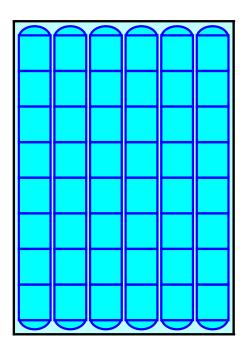
6 Rows x 77.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.25' Base Width 9.0" Stone Base + 45.0" Chamber Height + 12.0" Stone Cover = 5.50' Field Height

48 Chambers x 110.0 cf + 14.9 cf Cap Volume x 2 x 6 Rows = 5,456.5 cf Chamber Storage

15,347.2 cf Field - 5,456.5 cf Chambers = 9,890.7 cf Stone x 40.0% Voids = 3,956.3 cf Stone Storage

Chamber Storage + Stone Storage = 9,412.8 cf = 0.216 af Overall Storage Efficiency = 61.3% Overall System Size = 63.06' x 44.25' x 5.50'

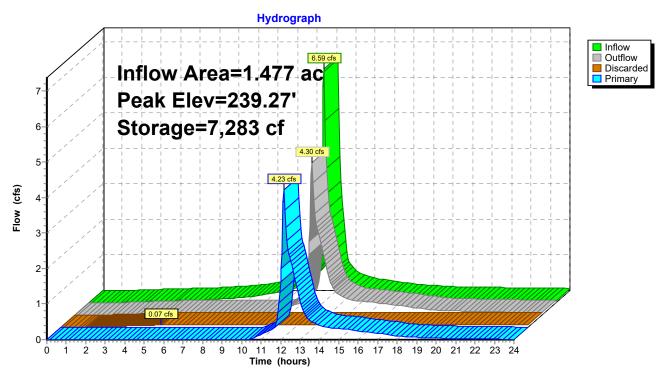
48 Chambers 568.4 cy Field 366.3 cy Stone





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#### Pond 5P: MC-3500



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## Summary for Link 1L: Ledin Avenue

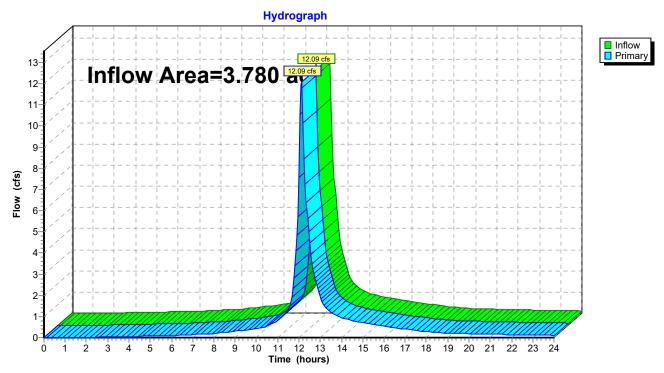
Inflow Area = 3.780 ac, 90.05% Impervious, Inflow Depth > 3.66" for 10-Year event

Inflow = 12.09 cfs @ 12.12 hrs, Volume= 1.152 af

Primary = 12.09 cfs @ 12.12 hrs, Volume= 1.152 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### Link 1L: Ledin Avenue



### Type III 24-hr 25-Year Rainfall=5.50"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-PR: 20 Ledin - Front of Runoff Area=26,398 sf 79.87% Impervious Runoff Depth>4.69"

Flow Length=275' Tc=6.0 min CN=93 Runoff=3.04 cfs 0.237 af

Subcatchment1B-PR: 20 Ledin - West Runoff Area=9,191 sf 25.59% Impervious Runoff Depth>2.95"

Flow Length=151' Slope=0.0200 '/' Tc=6.0 min CN=76 Runoff=0.72 cfs 0.052 af

Subcatchment1C-PR: 20 Ledin - Roof Runoff Area=42,427 sf 100.00% Impervious Runoff Depth>5.26"

Flow Length=279' Tc=6.0 min CN=98 Runoff=5.12 cfs 0.427 af

Subcatchment1D-PR: 20 Ledin - Rear Runoff Area=21,919 sf 94.62% Impervious Runoff Depth>5.03"

Flow Length=273' Tc=6.0 min CN=96 Runoff=2.61 cfs 0.211 af

Subcatchment1OFF-EX: 40 Ledin Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>5.14"

Flow Length=656' Tc=6.8 min CN=97 Runoff=7.63 cfs 0.637 af

**Pond 5P: MC-3500** Peak Elev=239.50' Storage=7,660 cf Inflow=7.73 cfs 0.638 af

Discarded=0.07 cfs 0.117 af Primary=5.77 cfs 0.470 af Outflow=5.84 cfs 0.587 af

Link 1L: Ledin Avenue Inflow=16.26 cfs 1.396 af

Primary=16.26 cfs 1.396 af

Total Runoff Area = 3.780 ac Runoff Volume = 1.563 af Average Runoff Depth = 4.96" 9.95% Pervious = 0.376 ac 90.05% Impervious = 3.404 ac

### Summary for Subcatchment 1A-PR: 20 Ledin - Front of Property

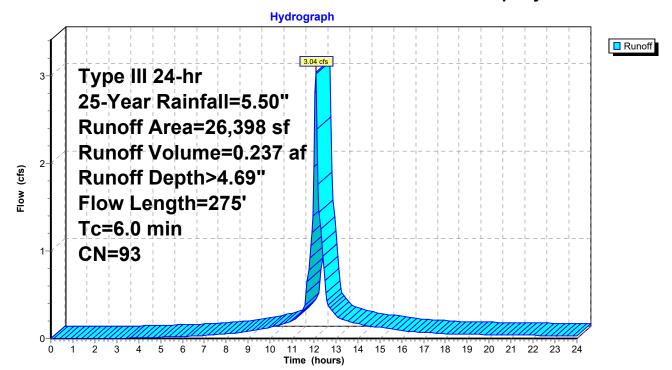
Runoff 3.04 cfs @ 12.09 hrs, Volume= 0.237 af, Depth> 4.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

_	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG B	
		4,008	69	50-75% Gra	ass cover, F	Fair, HSG B
		21,083	98	Paved park	ing, HSG B	
		26,398	93	Weighted A	verage	
		5,315		20.13% Per	vious Area	
		21,083		79.87% Imp	ervious Are	ea
	Тс	Length	Slope	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	4.54		Shallow Concentrated Flow, Front Parking Area and Road
_						Paved Kv= 20.3 fps
	5.3	275	Total,	Increased t	o minimum	Tc = 6.0 min

275 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1A-PR: 20 Ledin - Front of Property



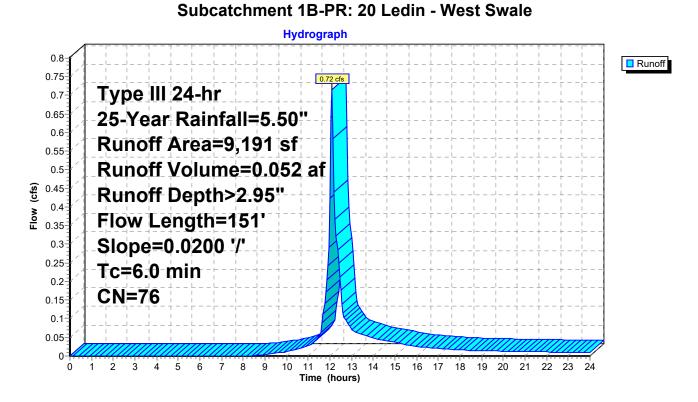
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### Summary for Subcatchment 1B-PR: 20 Ledin - West Swale

Runoff = 0.72 cfs @ 12.09 hrs, Volume= 0.052 af, Depth> 2.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN [	Description								
	6,839	69 5	50-75% Grass cover, Fair, HSG B								
	2,352	98 F	Paved park	ing, HSG B	3						
	9,191	76 \	Weighted Average								
	6,839	7	74.41% Per	vious Area							
	2,352	2	25.59% lmp	pervious Ar	ea						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description						
2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass						
					Short Grass Pasture Kv= 7.0 fps						
2.5	151	Total,	Increased t	o minimum	Tc = 6.0 min						



### Summary for Subcatchment 1C-PR: 20 Ledin - Roof Addition

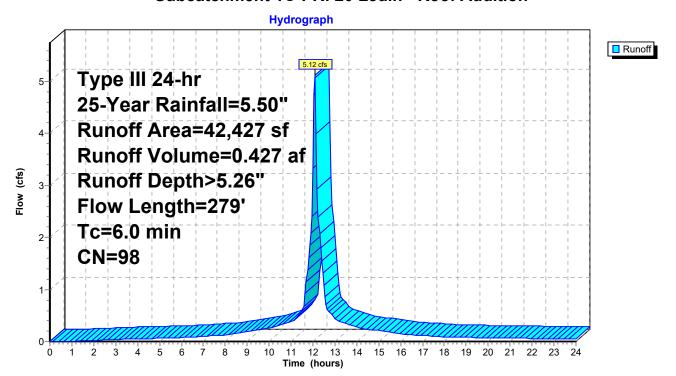
Runoff = 5.12 cfs @ 12.09 hrs, Volume= 0.427 af, Depth> 5.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

	Α	rea (sf)	CN D	escription		
		24,132	98 R	oofs, HSG	βB	
		18,295	98 R	oofs, HSC	3 B	
		42,427	98 V	Veighted A	verage	
		42,427	1	00.00% In	npervious A	vrea
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.7	196	0.0100	1.19		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	40	0.9900	44.78	15.63	Pipe Channel, Gutter
						8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'
						n= 0.010 PVC, smooth interior
	0.1	43	0.0250	9.32	7.32	Pipe Channel,
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
						0.040 5)/0 // // /
						n= 0.010 PVC, smooth interior

2.8 279 Total, Increased to minimum Tc = 6.0 min

#### Subcatchment 1C-PR: 20 Ledin - Roof Addition



### Summary for Subcatchment 1D-PR: 20 Ledin - Rear Developed

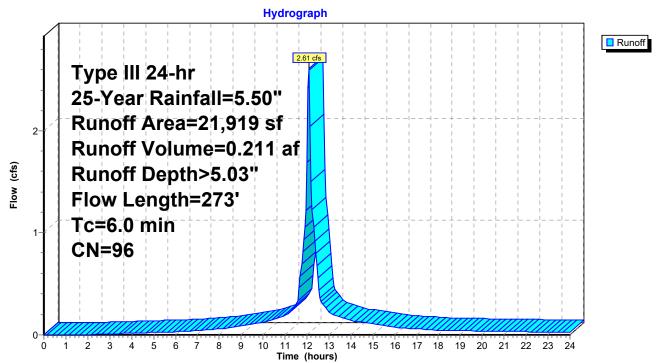
Runoff = 2.61 cfs @ 12.09 hrs, Volume= 0.211 af, Depth> 5.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

_	Α	rea (sf)	CN E	escription						
		1,179	69 5	50-75% Grass cover, Fair, HSG B						
_		20,740	98 F	aved park	ing, HSG B	3				
		21,919	96 V	Veighted A	verage					
		1,179	5	.38% Perv	ious Area					
		20,740	9	4.62% Imp	pervious Ar	ea				
	_									
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass				
						Short Grass Pasture Kv= 7.0 fps				
	0.4	74	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot				
						Paved Kv= 20.3 fps				
	8.0	48	0.0200	0.99		Shallow Concentrated Flow, 20 Ledin Grassed Area				
_						Short Grass Pasture Kv= 7.0 fps				
	37	272	Total I	neraced t	o minimum	Tc = 6.0 min				

3.7 273 Total, Increased to minimum Tc = 6.0 min

### Subcatchment 1D-PR: 20 Ledin - Rear Developed



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# Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 608% of capacity of segment #2

Runoff = 7.63 cfs @ 12.10 hrs, Volume= 0.637 af, Depth> 5.14"

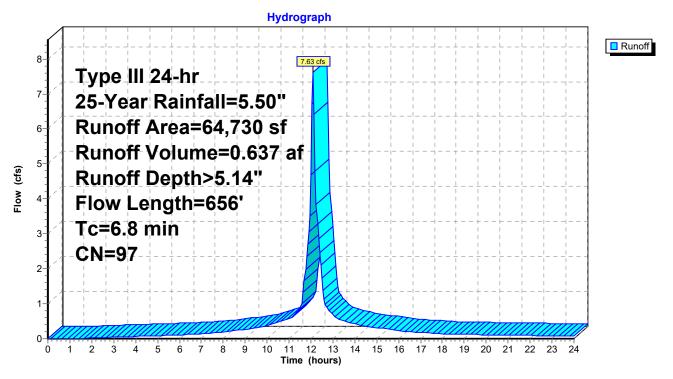
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

_	Α	rea (sf)	CN E	<b>Description</b>		
	27,051 98 Roofs, HSG B					
		3,049	79 <	50% Gras	s cover, Po	oor, HSG B
		34,630	98 F	aved park	ing, HSG E	3
		64,730	97 V	Veighted A	verage	
		3,049		.71% Perv	•	
		61,681	9	5.29% Imp	ervious Ar	ea
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
						4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
						n= 0.025 Corrugated metal
	0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
						Paved Kv= 20.3 fps
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
						Short Grass Pasture Kv= 7.0 fps
	1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
_						Paved Kv= 20.3 fps
	6.8	656	Total			

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## Subcatchment 10FF-EX: 40 Ledin



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## **Summary for Pond 5P: MC-3500**

Inflow Area = 1.477 ac, 98.17% Impervious, Inflow Depth > 5.18" for 25-Year event Inflow 7.73 cfs @ 12.09 hrs, Volume= 0.638 af 5.84 cfs @ 12.17 hrs, Volume= Outflow 0.587 af, Atten= 25%, Lag= 5.2 min Discarded = 0.07 cfs @ 4.25 hrs, Volume= 0.117 af Primary = 5.77 cfs @ 12.17 hrs, Volume= 0.470 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 239.50' @ 12.16 hrs Surf.Area= 2,790 sf Storage= 7,660 cf

Plug-Flow detention time= 97.5 min calculated for 0.586 af (92% of inflow) Center-of-Mass det. time= 56.1 min ( 806.7 - 750.6 )

Volume	Invert	Avail.Storage	Storage Description
#1A	235.50'	3,956 cf	44.25'W x 63.06'L x 5.50'H Field A
			15,347 cf Overall - 5,456 cf Embedded = 9,891 cf x 40.0% Voids
#2A	236.25'	5,456 cf	ADS_StormTech MC-3500 d +Capx 48 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			48 Chambers in 6 Rows
			Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf
		9,413 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	235.00'	<b>12.0" Round Culvert</b> L= 5.0' Ke= 1.000
	•		Inlet / Outlet Invert= 235.00' / 234.90' S= 0.0200 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf
#2			4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	236.75'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	237.50'	<b>8.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#5	Discarded	235.50'	1.020 in/hr Exfiltration over Surface area

**Discarded OutFlow** Max=0.07 cfs @ 4.25 hrs HW=235.56' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=5.65 cfs @ 12.17 hrs HW=239.47' (Free Discharge)

-1=Culvert (Inlet Controls 5.65 cfs @ 7.19 fps)

—2=Broad-Crested Rectangular Weir(Passes < 3.80 cfs potential flow)

-3=Orifice/Grate (Passes < 0.67 cfs potential flow)

4=Orifice/Grate (Passes < 2.15 cfs potential flow)

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#### Pond 5P: MC-3500 - Chamber Wizard Field A

# Chamber Model = ADS\_StormTechMC-3500 d +Cap (ADS StormTech® MC-3500 d rev 03/14 with Cap volume)

Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf

77.0" Wide + 9.0" Spacing = 86.0" C-C Row Spacing

8 Chambers/Row x 7.17' Long +1.85' Cap Length x 2 = 61.06' Row Length +12.0" End Stone x 2 = 63.06' Base Length

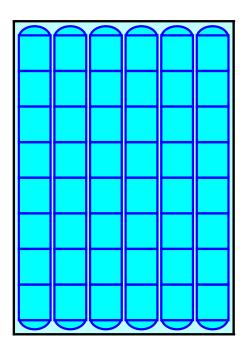
6 Rows x 77.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.25' Base Width 9.0" Stone Base + 45.0" Chamber Height + 12.0" Stone Cover = 5.50' Field Height

48 Chambers x 110.0 cf + 14.9 cf Cap Volume x 2 x 6 Rows = 5,456.5 cf Chamber Storage

15,347.2 cf Field - 5,456.5 cf Chambers = 9,890.7 cf Stone x 40.0% Voids = 3,956.3 cf Stone Storage

Chamber Storage + Stone Storage = 9,412.8 cf = 0.216 af Overall Storage Efficiency = 61.3% Overall System Size = 63.06' x 44.25' x 5.50'

48 Chambers 568.4 cy Field 366.3 cy Stone

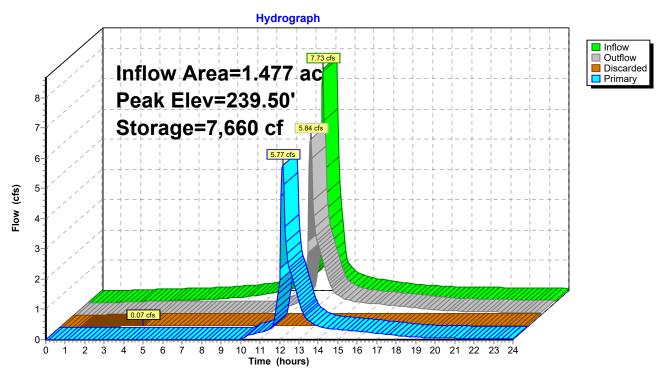




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### Pond 5P: MC-3500



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# Summary for Link 1L: Ledin Avenue

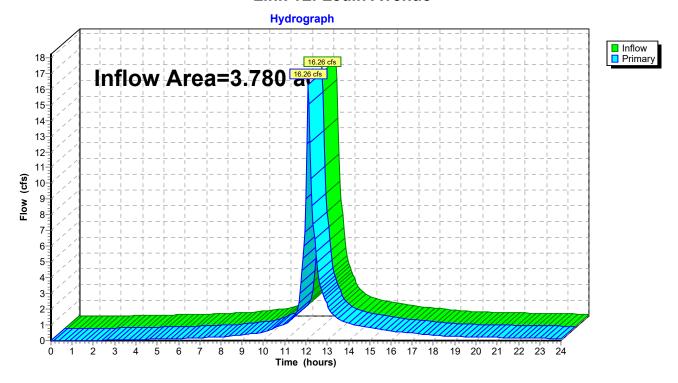
Inflow Area = 3.780 ac, 90.05% Impervious, Inflow Depth > 4.43" for 25-Year event

Inflow = 16.26 cfs @ 12.11 hrs, Volume= 1.396 af

Primary = 16.26 cfs @ 12.11 hrs, Volume= 1.396 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### **Link 1L: Ledin Avenue**



# Type III 24-hr 100-Year Rainfall=6.70"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A-PR: 20 Ledin - Front of Runoff Area=26,398 sf 79.87% Impervious Runoff Depth>5.87"

Flow Length=275' Tc=6.0 min CN=93 Runoff=3.76 cfs 0.296 af

Subcatchment1B-PR: 20 Ledin - West Runoff Area=9,191 sf 25.59% Impervious Runoff Depth>3.99"

Flow Length=151' Slope=0.0200 '/' Tc=6.0 min CN=76 Runoff=0.97 cfs 0.070 af

Subcatchment1C-PR: 20 Ledin - Roof Runoff Area=42,427 sf 100.00% Impervious Runoff Depth>6.46"

Flow Length=279' Tc=6.0 min CN=98 Runoff=6.25 cfs 0.524 af

Subcatchment1D-PR: 20 Ledin - Rear Runoff Area=21,919 sf 94.62% Impervious Runoff Depth>6.22"

Flow Length=273' Tc=6.0 min CN=96 Runoff=3.20 cfs 0.261 af

Subcatchment10FF-EX: 40 Ledin Runoff Area=64,730 sf 95.29% Impervious Runoff Depth>6.34"

Flow Length=656' Tc=6.8 min CN=97 Runoff=9.32 cfs 0.785 af

**Pond 5P: MC-3500** Peak Elev=240.19' Storage=8,507 cf Inflow=9.45 cfs 0.785 af

Discarded=0.07 cfs 0.120 af Primary=6.14 cfs 0.613 af Outflow=6.21 cfs 0.733 af

Link 1L: Ledin Avenue Inflow=19.87 cfs 1.764 af

Primary=19.87 cfs 1.764 af

Total Runoff Area = 3.780 ac Runoff Volume = 1.936 af Average Runoff Depth = 6.15" 9.95% Pervious = 0.376 ac 90.05% Impervious = 3.404 ac

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# Summary for Subcatchment 1A-PR: 20 Ledin - Front of Property

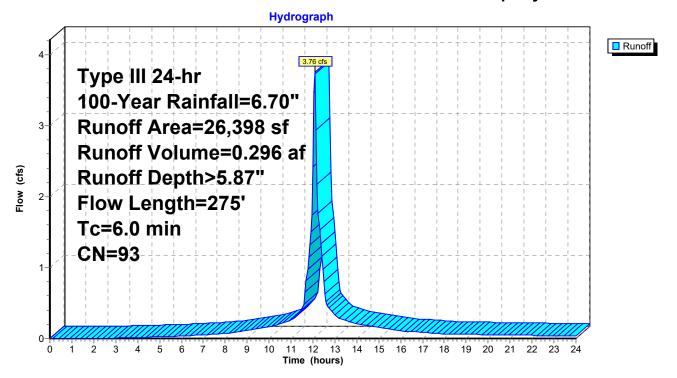
Runoff 3.76 cfs @ 12.09 hrs, Volume= 0.296 af, Depth> 5.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

_	Aı	rea (sf)	CN	Description		
		1,307	96	Gravel surfa	ace, HSG B	}
		4,008	69	50-75% Gra	ass cover, F	Fair, HSG B
		21,083	98	Paved park	ing, HSG B	
		26,398	93	Weighted A	verage	
		5,315		20.13% Per	-	
		21,083		79.87% Imp	ervious Are	ea
		,				
	Tc	Length	Slope	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	) (ft/sec)	(cfs)	·
	4.3	29	0.0340	0.11		Sheet Flow, Grassed Area
						Grass: Dense n= 0.240 P2= 3.20"
	0.2	39	0.0500	3.60		Shallow Concentrated Flow, Gravel
						Unpaved Kv= 16.1 fps
	8.0	207	0.0500	4.54		Shallow Concentrated Flow, Front Parking Area and Road
						Paved Kv= 20.3 fps
	5.3	275	Total,	Increased t	o minimum	Tc = 6.0 min

275 Total, Increased to minimum Tc = 6.0 min

# Subcatchment 1A-PR: 20 Ledin - Front of Property



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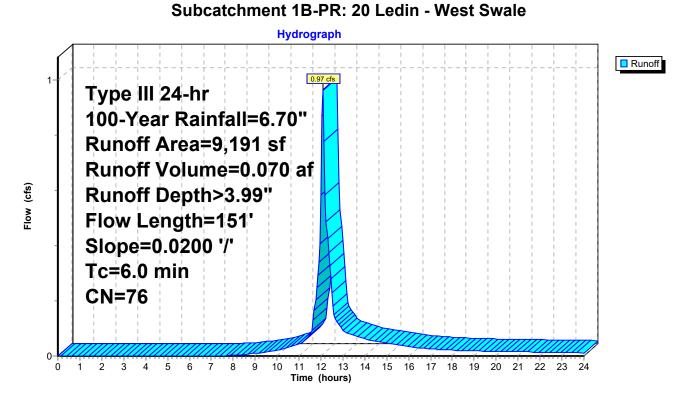
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# Summary for Subcatchment 1B-PR: 20 Ledin - West Swale

Runoff = 0.97 cfs @ 12.09 hrs, Volume= 0.070 af, Depth> 3.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

A	rea (sf)	CN I	Description						
	6,839	69 5	50-75% Gra	ass cover, f	Fair, HSG B				
	2,352	98 I	Paved park	Paved parking, HSG B					
	9,191	76 \	Weighted Average						
	6,839	7	74.41% Per	vious Area					
	2,352	2	25.59% lmp	pervious Ar	ea				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps				
2.5	151	Total,	Increased t	o minimum	Tc = 6.0 min				



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## Summary for Subcatchment 1C-PR: 20 Ledin - Roof Addition

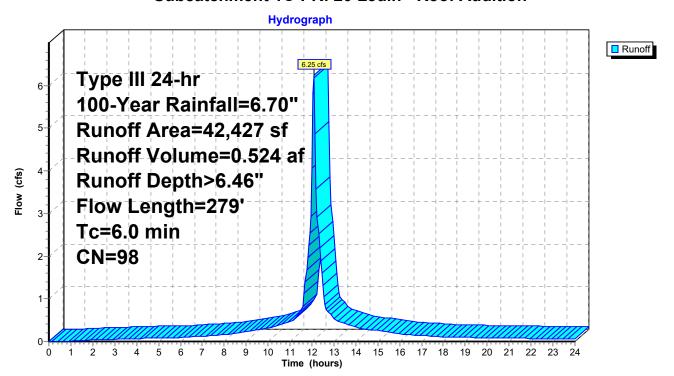
Runoff = 6.25 cfs @ 12.09 hrs, Volume= 0.524 af, Depth> 6.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

A	rea (sf)	CN D	escription		
	24,132	98 F	oofs, HSC	ВВ	
	18,295	98 F	Roofs, HSC	6 B	
	42,427	98 V	Veighted A	verage	
	42,427	1	00.00% In	npervious A	Area
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.7	196	0.0100	1.19		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.20"
0.0	40	0.9900	44.78	15.63	Pipe Channel, Gutter
					8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'
					n= 0.010 PVC, smooth interior
0.1	43	0.0250	9.32	7.32	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.010 PVC, smooth interior
- 0.0	070	<del> </del>	1.4		The Constitution

2.8 279 Total, Increased to minimum Tc = 6.0 min

#### Subcatchment 1C-PR: 20 Ledin - Roof Addition



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# Summary for Subcatchment 1D-PR: 20 Ledin - Rear Developed

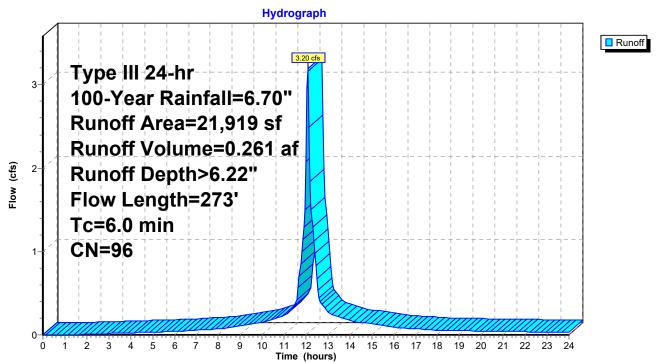
Runoff = 3.20 cfs @ 12.09 hrs, Volume= 0.261 af, Depth> 6.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

_	Α	rea (sf)	CN E	escription			
		1,179	69 50-75% Grass cover, Fair, HSG B				
_	20,740 98 Paved parking, HSG B					3	
		21,919	919 96 Weighted Average				
		1,179	5	.38% Perv	ious Area		
		20,740	9	4.62% Imp	pervious Ar	ea	
	_						
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass	
						Short Grass Pasture Kv= 7.0 fps	
0.4 74 0.0270 3.34			Shallow Concentrated Flow, 20 Ledin Parking Lot				
				Paved Kv= 20.3 fps			
	8.0	48	0.0200	0.99		Shallow Concentrated Flow, 20 Ledin Grassed Area	
_						Short Grass Pasture Kv= 7.0 fps	
	37	272	Total I	neraced t	o minimum	Tc = 6.0 min	

3.7 273 Total, Increased to minimum Tc = 6.0 min

# Subcatchment 1D-PR: 20 Ledin - Rear Developed



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# Summary for Subcatchment 10FF-EX: 40 Ledin

[47] Hint: Peak is 743% of capacity of segment #2

Runoff = 9.32 cfs @ 12.10 hrs, Volume= 0.785 af, Depth> 6.34"

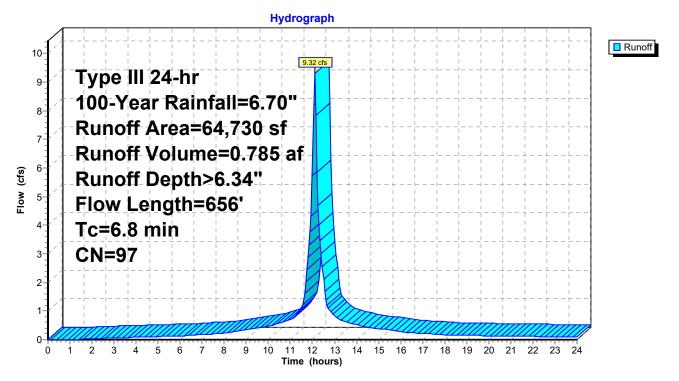
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

_	Α	rea (sf)	CN D	escription		
	27,051 98 Roofs, HSG B					
		3,049	79 <	50% Gras	s cover, Po	oor, HSG B
		34,630	98 P	aved park	ing, HSG E	3
		64,730	97 V	Veighted A	verage	
		3,049	4	.71% Perv	ious Area	
		61,681	9	5.29% Imp	ervious Ar	ea
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.6	184	0.0100	1.18		Sheet Flow, 40 Ledin Ave Rood
						Smooth surfaces n= 0.011 P2= 3.20"
	0.0	30	0.9900	11.28	1.25	Pipe Channel, Gutter
						4.0" x 4.0" Box Area= 0.1 sf Perim= 1.3' r= 0.08'
						n= 0.025 Corrugated metal
	0.7	93	0.0110	2.13		Shallow Concentrated Flow, Pavement
						Paved Kv= 20.3 fps
	2.5	151	0.0200	0.99		Shallow Concentrated Flow, Grass
						Short Grass Pasture Kv= 7.0 fps
	1.0	198	0.0270	3.34		Shallow Concentrated Flow, 20 Ledin Parking Lot
_						Paved Kv= 20.3 fps
	6.8	656	Total			

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#### Subcatchment 10FF-EX: 40 Ledin



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## **Summary for Pond 5P: MC-3500**

Inflow Area = 1.477 ac, 98.17% Impervious, Inflow Depth > 6.38" for 100-Year event Inflow 9.45 cfs @ 12.09 hrs, Volume= 0.785 af 6.21 cfs @ 12.18 hrs, Volume= Outflow 0.733 af, Atten= 34%, Lag= 5.7 min Discarded = 0.07 cfs @ 3.30 hrs, Volume= 0.120 af Primary = 6.14 cfs @ 12.18 hrs, Volume= 0.613 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 240.19' @ 12.18 hrs Surf.Area= 2,790 sf Storage= 8,507 cf

Plug-Flow detention time= 90.1 min calculated for 0.731 af (93% of inflow) Center-of-Mass det. time= 53.6 min ( 800.8 - 747.2 )

Volume	Invert	Avail.Storage	Storage Description
#1A	235.50'	3,956 cf	44.25'W x 63.06'L x 5.50'H Field A
			15,347 cf Overall - 5,456 cf Embedded = 9,891 cf x 40.0% Voids
#2A	236.25'	5,456 cf	ADS_StormTech MC-3500 d +Capx 48 Inside #1
			Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf
			Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap
			48 Chambers in 6 Rows
			Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf
		9,413 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	235.00'	<b>12.0" Round Culvert</b> L= 5.0' Ke= 1.000
	•		Inlet / Outlet Invert= 235.00' / 234.90' S= 0.0200 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf
#2			4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#3	Device 1	236.75'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#4	Device 1	237.50'	<b>8.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#5	Discarded	235.50'	1.020 in/hr Exfiltration over Surface area

**Discarded OutFlow** Max=0.07 cfs @ 3.30 hrs HW=235.56' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.07 cfs)

Primary OutFlow Max=6.12 cfs @ 12.18 hrs HW=240.16' (Free Discharge)

-1=Culvert (Inlet Controls 6.12 cfs @ 7.80 fps)

-2=Broad-Crested Rectangular Weir (Passes < 16.63 cfs potential flow)

-3=Orifice/Grate (Passes < 0.76 cfs potential flow)

4=Orifice/Grate (Passes < 2.56 cfs potential flow)

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#### Pond 5P: MC-3500 - Chamber Wizard Field A

# Chamber Model = ADS\_StormTechMC-3500 d +Cap (ADS StormTech® MC-3500 d rev 03/14 with Cap volume)

Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap Cap Storage= +14.9 cf x 2 x 6 rows = 178.8 cf

77.0" Wide + 9.0" Spacing = 86.0" C-C Row Spacing

8 Chambers/Row x 7.17' Long +1.85' Cap Length x 2 = 61.06' Row Length +12.0" End Stone x 2 = 63.06' Base Length

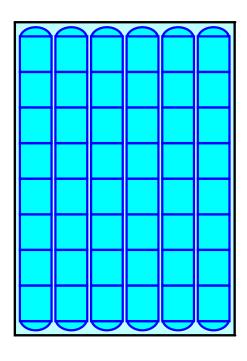
6 Rows x 77.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.25' Base Width 9.0" Stone Base + 45.0" Chamber Height + 12.0" Stone Cover = 5.50' Field Height

48 Chambers x 110.0 cf + 14.9 cf Cap Volume x 2 x 6 Rows = 5,456.5 cf Chamber Storage

15,347.2 cf Field - 5,456.5 cf Chambers = 9,890.7 cf Stone x 40.0% Voids = 3,956.3 cf Stone Storage

Chamber Storage + Stone Storage = 9,412.8 cf = 0.216 af Overall Storage Efficiency = 61.3% Overall System Size = 63.06' x 44.25' x 5.50'

48 Chambers 568.4 cy Field 366.3 cy Stone

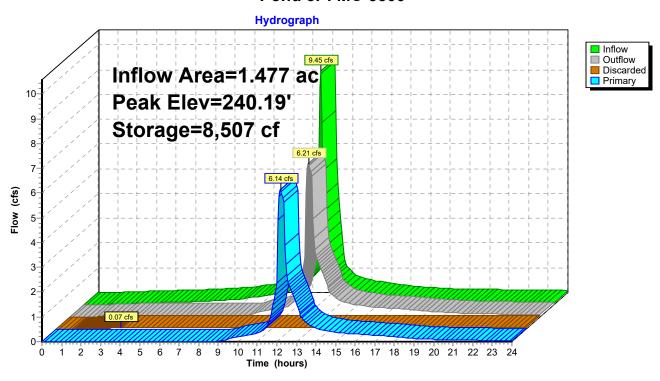




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Pond 5P: MC-3500



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# Summary for Link 1L: Ledin Avenue

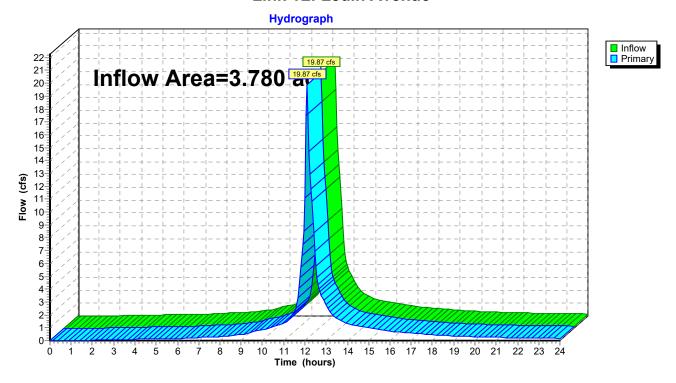
Inflow Area = 3.780 ac, 90.05% Impervious, Inflow Depth > 5.60" for 100-Year event

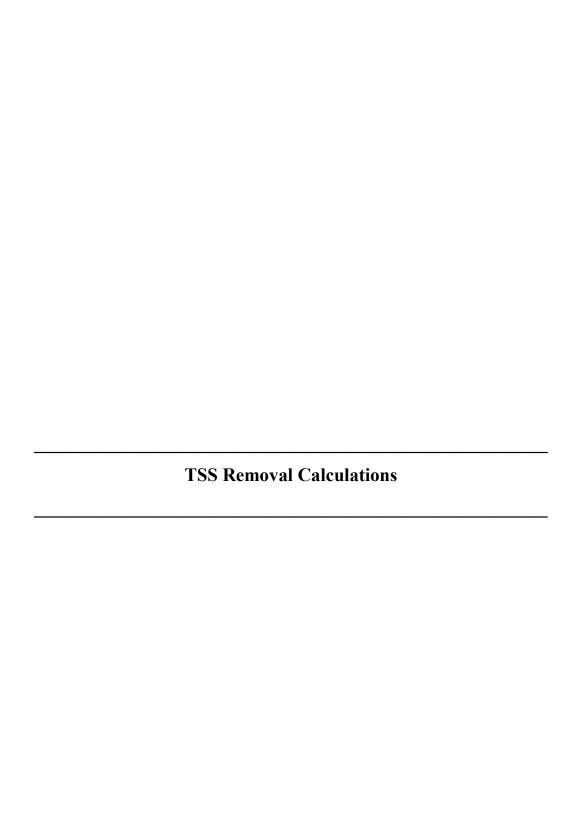
Inflow = 19.87 cfs @ 12.10 hrs, Volume= 1.764 af

Primary = 19.87 cfs @ 12.10 hrs, Volume= 1.764 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### **Link 1L: Ledin Avenue**





INSTRUCTIONS: Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

	Location	Out at the out 4D DD /D	D		
	Location:	Subcatchment 1D-PR (Re	ear Pavement Area)		
	В	С	D	Е	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
•	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
oval	Deep Sump and Hooded Catch Basin Proprietary Water Quality Unit	0.80	0.75	0.60	0.15
4		0.25	0.15	0.04	0.11
TSS	Stormtech Isolator Row  Subsurface Infiltration Structure	0.80	0.11	0.09	0.02
Č	2	0.00	0.02	0.00	0.02
		Total T	SS Removal =	98%	Separate Form Needs to be Completed for Each Outlet or BMP Train
	Project:	20 Ledin Avenue, Avon, M	IA		_
	Prepared By:	KPS		*Equals remaining load from	n previous BMP (E)
	Date:	4/23/2021		which enters the BMP	

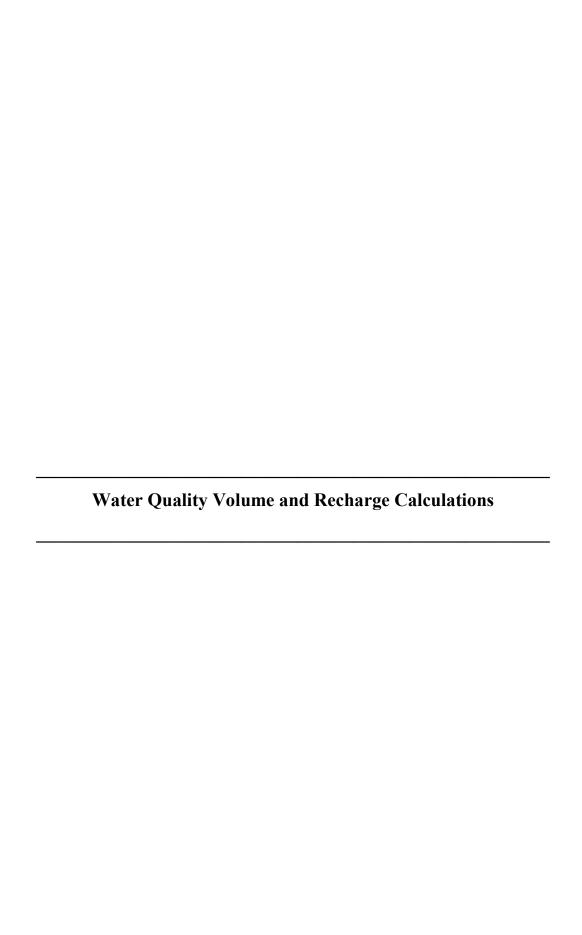
<sup>\*\*</sup> Stormtech Isolator Row conservatively assumed to provide a minimum of 25% TSS removal

INSTRUCTIONS: Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

				, ,		
		Location:	Subcatchment 10FF-EX &	1B-PR (Adjacent property	and small paved area)	
		D	0	D	_	-
		В	C	D Starting TSS	E	F
		BMP <sup>1</sup>	TSS Removal Rate <sup>1</sup>	Starting TSS	Amount	Remaining
	İ	DIVIP	Rate	Load*	Removed (C*D)	Load (D-E)
	)t	Deep Sump and Hooded				
	)e(	Catch Basin	0.25	1.00	0.25	0.75
æ	<b>Calculation Worksheet</b>	Proprietary Water Quality				
TSS Removal	ork	Unit	0.80	0.75	0.60	0.15
Ĕ	Š					
<b>Re</b>	<b>D</b>		0.00	0.15	0.00	0.15
S	tio		0.00	0.15	0.00	0.15
Ś	ıla					
	CL		0.00	0.15	0.00	0.15
	à					
	J		0.00	0.15	0.00	0.15
						Separate Form Needs to
			Total T	SS Removal =	85%	be Completed for Each Outlet or BMP Train
		Project:	20 Ledin Avenue, Avon, M		05/0	
		Prepared By:		A	] *Equals remaining load froi	m nrevious RMP (F)
		•	4/23/2021		which enters the BMP	ii pievious bivii (L)
		240.			The second second second	

<sup>\*\*</sup> Stormtech Isolator Row conservatively assumed to provide a minimum of 25% TSS removal





# Water Quality Volume Flow Rate Calculations

Project Name: Ledin Avenue Building Expansion Date: 4/23/2021

Project Location: 20 Ledin Avenue, Avon, MA Calculated By: KPS

Project Number: 311-399 Checked By: KPS

Structure Name: WQU A2 Description: Stormceptor STC 900

Subcatchment: 1B-PR & 10FF-EX Total Drainage Area: 73,933 sq ft

1.70 ac

Total Impervious Area\*: 36,981 sq ft \* Clean Roof Areas Excluded

0.85 ac from Impervious

Area

Runoff Depth to be Treated: 1.0 inches

Required Water Quality Volume: 0.071 ac ft 3082 cf

#### **FLOW RATE CONVERSION**

Q = (qu)(A)(WQV)

Where:

Q = flow rate associated with the 1-inch of runoff, in cfs

qu = the unit peak discharge, in csm/in.

A = impervious surface drainage area, in square miles

WQV = water quality volume in watershed inches

Given:

1-acre =  $0.0015625 \text{ mi}^2$ 5 minute = 0.083 hoursqu (1/2-inch) = 773 csm/in

Calculation:

qu= **773** A= 0.85 ac WQV= 1.0 in

Required Water Quality Flow Rate: 1.03 cfs

Stormceptor STC 2400 will provide 80% TSS Removal Efficiency for flows up to 1.58 cfs

(Based on Manufacturer's sizing. See attached calculation.)

<sup>\*</sup> Flow rate conversion based on the Massachusetts Department of Environmental Protection Wetlands Program - Standard Method to Convert Required Water Quality Volume to a Discharge Rate for Sizing Flow Based Manufactured Proprietary Stormwater Treatment Practices



# Water Quality Volume Flow Rate Calculations

Project Name: Ledin Avenue Building Expansion Date: 4/23/2021

Project Location: 20 Ledin Avenue, Avon, MA Calculated By: KPS

Project Number: 311-399 Checked By: KPS

Structure Name: WQU A-1 Description: Stormceptor STC 900

Subcatchment: 1D-PR Total Drainage Area: 21,919 sq ft

0.50 ac

Total Impervious Area: 20,740 sq ft

0.48 ac

Runoff Depth to be Treated: 1.0 inches

Required Water Quality Volume: 0.040 ac ft 1729 cf

#### **FLOW RATE CONVERSION**

Q = (qu)(A)(WQV)

Where:

Q = flow rate associated with the 1/2-inch of runoff, in cfs

qu = the unit peak discharge, in csm/in.

A = impervious surface drainage area, in square miles

WQV = water quality volume in watershed inches

Given:

1-acre =  $0.0015625 \text{ mi}^2$ 5 minute = 0.083 hoursqu (1/2-inch) = 773 csm/in

Calculation:

qu= **773** A= 0.48 ac WQV= 1.0 in

Required Water Quality Flow Rate: 0.58 cfs

Stormceptor STC 900 will provide 80% TSS Removal Efficiency for flows up to 0.89 cfs

Subsurface Infiltration Chambers provide 2,011 cf of storage below low flow outlet exceeding WQV Requirement

(Based on Manufacturer's sizing. See attached calculation.)

<sup>\*</sup> Flow rate conversion based on the Massachusetts Department of Environmental Protection Wetlands Program - Standard Method to Convert Required Water Quality Volume to a Discharge Rate for Sizing Flow Based Manufactured Proprietary Stormwater Treatment Practices



# Groundwater Recharge Calculations

Project Name: Ledin Avenue Building Expansion

Project Location: 20 Ledin Avenue, Avon, MA

Project Number: 311-399

Date: 4/23/2021
Calculated By: KPS
Checked By: WG

#### **Existing Conditions Impervious Area**

Hydraulic		Area	Recharge	Volume
Soil Group	(sq ft)	(acres)	Depth (in)	(cu ft)
Α	0	0.00	0.60	0.0
В	53,608	1.23	0.35	1563.6
С	0	0.00	0.25	0.0
D	0	0.00	0.10	0.0
TOTAL	53,608	1.23		1,564

#### **Proposed Conditions Impervious Area**

Hydraulic		Area	Recharge	Volume
Soil Group	(sq ft)	(acres)	Depth (in)	(cu ft)
А	0	0.00	0.60	0.0
В	86,591	1.99	0.35	2525.6
С		0.00	0.25	0.0
D	0	0.00	0.10	0.0
TOTAL	86,591	1.99		2,526

Net Required 962 cu ft Recharge Volume:

#### **Capture Area Adjustment**

\* Impervious Area to Recharge Facility: 1.45 ac Total Site Impervious Area: 1.99 ac

\*\* Impervious Ratio: 1.37

\* (includes portions of the pavement and the entire

root )

\*\* (Total Site Impervious / Impervious Area to Recharge Facility)

Adjusted Required
Recharge Volume: 1,319 cu ft

#### **Provided Recharge Volume**

Subcatchment 1D 2,011 cf

MC3500 Stormtech Chambers (see attached HydroCAD analysis)

Total Provided

Recharge Volume: 2,011 cu ft

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# Stage-Area-Storage for Pond 5P: MC-3500

Elevation	Surface	Storage	Elevation	Surface	Storage	
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)	
235.50	2,790	0	236.54	2,790	1,521	
235.52	2,790	22	236.56	2,790	1,568	
235.54	2,790	45	236.58	2,790	1,614	
235.56	2,790	67	236.60	2,790	1,661	
235.58	2,790	89	236.62	2,790	1,708	
235.60	2,790	112	236.64	2,790	1,755	
235.62	2,790	134	236.66	2,790	1,801	
235.64	2,790	156	236.68	2,790	1,848	
235.66	2,790	179	236.70	2,790	1,895	
235.68	2,790	201	236.72	2,790	1,941	
235.70	2,790	223	236.74	2,790	1,988	7
235.72	2,790	246	236.76	2,790	2,034	
235.74	2,790	268	236.78	2,790	2,081	
235.76	2,790	290	236.80	2,790	2,127	
235.78	2,790	313	236.82	2,790	2,173	
235.80	2,790	335	236.84	2,790	2,220	
235.82	2,790	357	236.86	2,790	2,266	
235.84	2,790	379	236.88	2,790	2,312	PROVIDED STORAGE
235.86	2,790	402	236.90	2,790	2,359	BELOW OVERFLOW
235.88	2,790	424	236.92	2,790	2,405	
235.90	2,790	446	236.94	2,790	2,451	ELEVATION = 2,011 CF
235.92	2,790	469	236.96	2,790	2,497	
235.94	2,790	491	236.98	2,790	2,543	
235.96	2,790	513	237.00	2,790	2,589	
235.98	2,790	536	237.02	2,790	2,635	
236.00	2,790	558	237.04	2,790	2,681	
236.02	2,790	580	237.06	2,790	2,726	
236.04	2,790	603	237.08	2,790	2,772	
236.06	2,790	625	237.10	2,790	2,818	
236.08	2,790	647	237.12	2,790	2,864	
236.10	2,790	670	237.14	2,790	2,909	
236.12	2,790	692	237.16	2,790	2,955	
236.14	2,790	714	237.18	2,790	3,000	
236.16	2,790	737	237.20	2,790	3,046	
236.18	2,790	759	237.22	2,790	3,091	
236.20	2,790	781	237.24	2,790	3,137	
236.22	2,790	804	237.26	2,790	3,182	
236.24	2,790	826	237.28	2,790	3,227	
236.26	2,790	861	237.30	2,790	3,272	
236.28	2,790	908	237.32	2,790	3,317	
236.30	2,790	955	237.34	2,790	3,363	
236.32	2,790	1,003	237.36	2,790	3,408	
236.34	2,790	1,050	237.38	2,790	3,453	
236.36	2,790	1,097	237.40	2,790	3,497	
236.38	2,790	1,145	237.42	2,790	3,542	
236.40	2,790	1,192	237.44	2,790	3,587	
236.42	2,790	1,239	237.46	2,790	3,632	
236.44	2,790	1,286	237.48	2,790	3,677	
236.46	2,790	1,333	237.50	2,790	3,721	
236.48	2,790	1,380	237.52	2,790	3,766	
236.50	2,790	1,427	237.54	2,790	3,810	
236.52	2,790	1,474	237.56	2,790	3,855	
		•				

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# Stage-Area-Storage for Pond 5P: MC-3500 (continued)

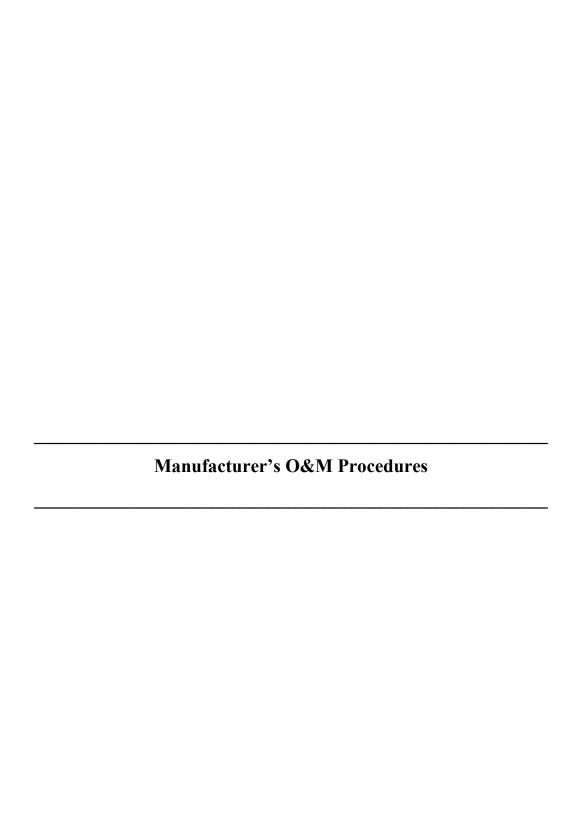
□1	0	04		0	04
Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
237.58	2,790	3,899	238.62	2,790	6,089
237.60	2,790	3,943	238.64	2,790	6,129
237.62	2,790	3,987	238.66	2,790	6,168
237.64	2,790	4,032	238.68	2,790	6,207
237.66	2,790	4,076	238.70	2,790	6,246
237.68	2,790	4,120	238.72	2,790	6,285
237.70	2,790	4,164	238.74	2,790	6,323
237.72	2,790	4,207	238.76	2,790	6,362
237.74	2,790	4,251	238.78	2,790	6,400
237.76	2,790	4,295	238.80	2,790	6,438
237.78	2,790	4,338	238.82	2,790	6,476
237.80	2,790	4,382	238.84	2,790	6,514
237.82	2,790	4,425	238.86	2,790	6,552
237.84	2,790	4,469	238.88	2,790	6,590
237.86	2,790	4,512	238.90	2,790	6,627
237.88	2,790	4,555	238.92	2,790	6,664
237.90	2,790	4,599	238.94	2,790	6,702
237.92	2,790	4,642	238.96	2,790	6,739
237.94	2,790	4,685	238.98	2,790	6,775
237.96	2,790	4,728	239.00	2,790	6,812
237.98	2,790	4,770	239.02	2,790	6,848
238.00	2,790	4,813	239.04	2,790	6,885
238.02	2,790	4,856	239.06	2,790	6,921
238.04	2,790	4,898	239.08	2,790	6,957
238.06	2,790	4,941	239.10	2,790	6,992
238.08	2,790	4,983	239.12	2,790	7,028
238.10	2,790	5,025	239.14	2,790	7,063
238.12	2,790	5,068	239.16	2,790	7,098
238.14	2,790	5,110	239.18	2,790	7,133
238.16	2,790	5,152	239.20	2,790	7,168
238.18	2,790	5,194	239.22	2,790	7,202
238.20	2,790	5,236	239.24	2,790	7,237
238.22	2,790	5,277	239.26	2,790	7,271
238.24	2,790	5,319	239.28	2,790	7,305
238.26	2,790	5,360	239.30	2,790	7,338
238.28	2,790	5,402	239.32	2,790	7,371
238.30	2,790	5,443	239.34	2,790	7,405
238.32	2,790	5,484	239.36	2,790	7,437
238.34	2,790	5,526	239.38	2,790	7,470
238.36	2,790	5,567	239.40	2,790	7,502
238.38	2,790	5,607	239.42	2,790	7,534
238.40	2,790	5,648	239.44	2,790	7,566
238.42	2,790	5,689	239.46	2,790	7,597
238.44	2,790	5,730	239.48	2,790	7,628
238.46	2,790	5,770	239.50	2,790	7,659
238.48	2,790	5,810	239.52	2,790	7,689
238.50	2,790	5,851	239.54	2,790	7,718
238.52	2,790	5,891	239.56	2,790	7,748
238.54	2,790	5,931	239.58	2,790	7,776
238.56	2,790	5,970	239.60	2,790	7,805
238.58	2,790	6,010	239.62	2,790	7,832
238.60	2,790	6,050	239.64	2,790	7,860

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# Stage-Area-Storage for Pond 5P: MC-3500 (continued)

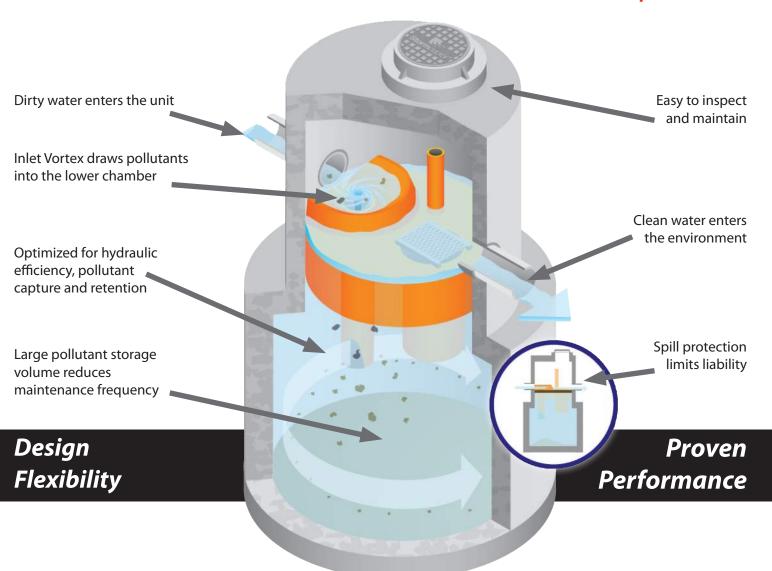
Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
239.66	2,790	7,886	240.70	2,790	9,078
239.68	2,790	7,913	240.72	2,790	9,100
239.70	2,790	7,938	240.74	2,790	9,123
239.72	2,790	7,964	240.76	2,790	9,145
239.74	2,790	7,989	240.78	2,790	9,167
239.76	2,790	8,014	240.80	2,790	9,190
239.78	2,790	8,038	240.82	2,790	9,212
239.80	2,790	8,063	240.84	2,790	9,234
239.82	2,790	8,087	240.86	2,790	9,257
239.84	2,790	8,111	240.88	2,790	9,279
239.86	2,790	8,135	240.90	2,790	9,301
239.88	2,790	8,159	240.92	2,790	9,323
239.90	2,790	8,182	240.94	2,790	9,346
239.92	2,790	8,206	240.96	2,790	9,368
239.94	2,790	8,229	240.98	2,790	9,390
239.96	2,790	8,252	241.00	2,790	9,413
239.98	2,790	8,274			•
240.00	2,790	8,297			
240.02	2,790	8,319			
240.04	2,790	8,341			
240.06	2,790	8,364			
240.08	2,790	8,386			
240.10	2,790	8,408			
240.12	2,790	8,431			
240.14	2,790	8,453			
240.16	2,790	8,475			
240.18	2,790	8,498			
240.20	2,790	8,520			
240.22	2,790	8,542			
240.24	2,790	8,565			
240.26	2,790	8,587			
240.28	2,790	8,609			
240.30	2,790	8,631			
240.32	2,790	8,654			
240.34	2,790	8,676			
240.36	2,790	8,698			
240.38	2,790	8,721			
240.40	2,790	8,743			
240.42	2,790	8,765			
240.44	2,790	8,788			
240.46	2,790	8,810			
240.48	2,790	8,832			
240.50	2,790	8,855			
240.52	2,790	8,877			
240.54	2,790	8,899			
240.56	2,790	8,922			
240.58	2,790	8,944			
240.60	2,790	8,966			
240.62	2,790	8,989			
240.64	2,790	9,011			
240.66	2,790	9,033			
240.68	2,790	9,056			





# **Stormwater Treatment Made Simple!**

TSS & Oil Removal Scour Prevention Small Footprint



Environmentally Engineered Stormwater Solutions... that exceed your client's needs!





Stormceptor® is an underground stormwater quality treatment device that is unparalleled in its effectiveness for pollutant capture and retention. With thousands of systems operating worldwide, Stormceptor delivers protection every day in every storm.

With patented technology, optimal treatment occurs by allowing free oil to rise and sediment to settle. The Stormceptor design prohibits scour and release of previously captured pollutants, ensuring superior treatment and protection during even the most extreme storm events.

Stormceptor is very easy to design and provides flexibility under varying site constraints such as tight right-of-ways, zero lot lines and retrofit projects. Design flexibility allows for a cost-effective approach to stormwater treatment. Stormceptor has proven performance backed by the longest record of lab and field verification in the industry.

# **Tested Performance**

■ Fine particle capture

■ Prevents scour or release

95%+ Oil removal

# Massachusetts - Water Quality (Q) Flow Rate

Stormceptor STC Model	Inside Diameter	Typical Depth Below Inlet Pipe Invert <sup>1</sup>	Water Quality Flow Rate Q <sup>2</sup>	Peak Conveyance Flow Rate <sup>3</sup>	Hydrocarbon Capacity ⁴	Maximum Sediment Capacity <sup>4</sup>
	(ft)	(in)	(cfs)	(cfs)	(Gallons)	(ft³)
STC 450i	4	68	0.40	5.5	86	46
STC 900	6	63	0.89	22	251	89
STC 2400	8	104	1.58	22	840	205
STC 4800	10	140	2.47	22	909	543
STC 7200	12	148	3.56	22	1,059	839
STC 11000	2 x 10	142	4.94	48	2,792	1,086
STC 16000	2 x 12	148	7.12	48	3,055	1,677

<sup>&</sup>lt;sup>1</sup> Depth Below Pipe Inlet Invert to the Bottom of Base Slab, and Maximum Sediment Capacity can vary to accommodate specific site designs and pollutant loads. Depths can vary to accommodate special designs or site conditions. Contact your local representative for assistance.

<sup>&</sup>lt;sup>4</sup> Hydrocarbon & Sediment capacities can be modified to accommodate specific site design requirements, contact your local representative for assistance.



<sup>&</sup>lt;sup>2</sup> Water Quality Flow Rate (Q) is based on 80% annual average TSS removal of the OK110 particle size distribution.

<sup>&</sup>lt;sup>3</sup> Peak Conveyance Flow Rate is based upon ideal velocity of 3 feet per second and outlet pipe diameters of 18-inch, 36-inch, and 54-inch diameters.



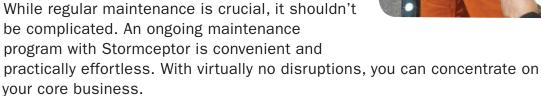
# Inspection and Maintenance. Easy. Convenient.

When it rains, oils, sediment and other contaminants are captured and contained by over 20,000 Stormceptor units operating worldwide. While Stormceptor's patented scour prevention technology ensures captured pollutants remain in the unit during all rainfall events, the accumulated pollutants must eventually be removed as part of a regular maintenance program.

If neglected, oil and sediment gradually build up and diminish any BMP's efficiency, harming the environment and leaving owners and operators vulnerable to fines, surcharges and bad publicity.

#### Maintenance is a must

Ease, frequency and cost of maintenance are often overlooked by specifiers when considering the merits of a stormwater treatment system. In reality, maintenance is fundamental to the long-term performance of any stormwater quality treatment device.





Inspections are easily carried out above ground from any standard surface access cover through a visual inspection of the orifice and drop tee components. A sludge judge and oil dip-stick are all that are needed for sediment and oil depth measurements.

# **Easy unit access**

Maintenance is typically conducted from the same surface access cover, eliminating the need for confined space entry into the unit. Your site remains undisturbed, saving you time and money.







# No muss, no fuss and fast

Maintenance is performed quickly and inexpensively with a standard vacuum truck. Servicing usually takes less than two hours, with no disruption to your site.

A complete stormwater management plan for Stormceptor extends beyond installation and performance to regular maintenance. It's the smart, cost-effective way to ensure your unit continues to remove more pollutants than any other separator for decades to come.

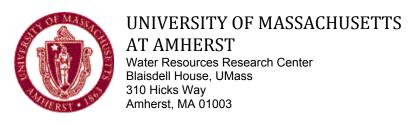


# **Stormceptor maintenance recommendations**

- Units should be inspected post-construction, prior to being put into service.
- Inspect every six months for the first year of operation to determine the oil and sediment accumulation rate.
- In subsequent years, inspections can be based on first-year observations or local requirements.
- Cleaning is required once the sediment depth reaches 15% of storage capacity, (generally taking one year or longer). Local regulations for maintenance frequency may vary.
- Inspect the unit immediately after an oil, fuel or chemical spill.
- A licensed waste management company should remove captured petroleum waste products from any oil, chemical or fuel spills and dispose responsibly.

With over 20,000 units operating worldwide, Stormceptor performs and protects every day, in every storm.





Massachusetts Stormwater Evaluation Project

(413) 545-5532 (413) 545-2304 FAX www.mastep.net

# **MASTEP Technology Review**

**Technology Name:** Stormceptor

Studies Reviewed: Final NJCAT Technology Verification Stormceptor STC900 September 2004;

Coventry University Study, 1996; Technology Assessment, University of

Massachusetts, 1997; SeaTac Stormceptor Performance report 2001; SWAMP report Ontario 2004; Phoenix Group Edmonton report 1995; Stormceptor 1200 Field Evaluation report 2004; Applied Hydrology Associates Denver report 2003; Rinker Materials Como Park St. Paul MN report 2002: VA DOT / UVA "Testing of Ultra-

Urban Stormwater Best Management Practices" report 2001.

Hydrodynamic Separator Sediment Retention Testing, Mohseni, 2010.

Date: September 17, 2013

**Reviewer**: Jerry Schoen

Rating: 2

Brief rationale for rating: This rating is primarily based on the 2005 NJCAT Technology Verification study. In general, this was a well-conducted test, which in large part followed NJDEP test guidelines for laboratory studies, which MASTEP considers as the laboratory equivalent of TARP field protocols. Issues of concern: the study measured suspended sediment concentration (SSC) rather than total suspended solids (TSS). Although SSC is considered by many scientists to be the preferred method, it is at odds with Massachusetts stormwater regulations, which are based on TSS treatment. Comparing SSC and TSS results is considered an inexact science. The test was conducted with higher influent sediment concentrations than is preferred, but results were fairly consistent across all ranges studied. The particle size distribution also appears to be slightly higher than the target test range. There are additional field studies that in general support the results obtained in this laboratory studies. These studies do not satisfy TARP protocols, but they do not contradict results obtained in the NJCAT study.

#### **TARP Requirements Not Met\*:**

- Measurements in TSS.
- Influent sediment concentration is 100 300 mg/l: actual was 153-460.
- No documentation of a Quality Assurance Project Plan
- Third party studies are preferred. This was conducted by Stormceptor personnel, with sample analyses conducted by an external laboratory.

#### Other Comments:

\* The 2010 Mohseni study evaluates the susceptibility of the Stormceptor to scouring, or washout of collected sediments. Report concluded that the unit does not scour at high flows as long as sediment depth does not exceed maintenance level.

<sup>\*</sup> Criteria also based on NIDEP laboratory testing guidelines.



#### MASTEP Technology Review

Massachusetts Stormwater Evaluation Project (413) 545-5532 (413) 545-2304 FAX www.mastep.net

Technology Name: Isolator Row

Studies Reviewed: Christensen, Andrew and Vince Neary. Hydraulic Performance and Sediment

Trap Efficiency for the StormTech SC-740 Isolator Row. Tennessee

Technological University, February 2005.

Neary, Vincent, PhD. Performance Evaluation of Sediment Removal Efficiency Stormtech Isolator Row. Tennessee Tech University. October 20, 2006.

New Jersey Corporation for Advanced Technology. NJCAT Verification

of the StormTech Isolator Row. August 2007.

University of New Hampshire Stormwater Center. Final Report on Field Verification Testing of the Stormtech Isolator Row Treatment Unit. Submitted to

StormTech LLC June 2008.

University of New Hampshire Stormwater Center. Performance Evaluation Report on

of the Stormtech Isolator Row Treatment Unit. September 2010

**Date:** January 14, 2012

**Reviewers:** Sarah Titus, updated by Jerry Schoen

Rating: 2

#### Brief rationale for rating:

The Isolator Row was tested in the field by the UNH Stormwater Center and in the lab by Tennessee Tech University. Field testing monitored 23 events over two years, sampling 13.2" rainfall or about 27% of the annual average. This study was done under a QAPP that was designed to substantially meet TARP and TAPE requirements.

Lab testing examined sediment removal for three different influent mixes; the SIL-CO-SIL 106, SIL-CO-SIL 250 and the OK-110 silica. Across all influent mixes, 21 test runs were done and 14 flow rates were tested at average influent concentrations from 164-424mg/l. NJCAT was able to use the runs to extrapolate the data to calculate weighted removal efficiencies for 25, 50, 75, 100 and 125% of treatment operating rate. Claims for each influent mix were verified by NJCAT. While all of these studies met many requirements necessary for TARP there was no scour testing, statistical analysis or QC data presented for any study. The laboratory studies did not use a certified lab and the one micron filter sock at the outlet was only partially effective at trapping the finer particles from the flow stream. This led to increasing influent and effluent SSC values as the detention time went up during the course of each test run. Removal rates for earlier samples were higher than later samples in the same run.

#### Requirements not met:

- No discussion of QC test results.
- Sampled <50% of average annual rainfall and less than minimum 13" required total in the field
- No discussion of scour testing

#### Other comments:

Field study:

- d50 influent particle size 44 microns.
- Effective TSS, SSC, Zinc, total phosphorus, total petroleum hydrocarbon reported throughout study period.
- Zinc and TP removal efficiency improved over the course of the study, presumably due to build of an
  organic filter cake on system's fabric. However, this buildup may also lead to increased incidence of
  bypass in larger storms. This may be a consideration for maintenance planning.
- Negative removal rates for dissolved inorganic nitrogen, suggesting this system is not effective at treating dissolved nitrogen.

#### Lab study:

- Particle size distributions: OK 110 d50=110, SIL CO SIL 106 d50=22, SIL CO SIL 250= 45 microns.
   In the field the d50 was measured as 0.038mm.
- Flow rates tested in the lab at treatment flow rates from 0.1-1.2cfs. SIL CO SIL 106 was tested at 3.2gpm/ft2 and SIL CO SIL 250 was tested at 3.2 (0.4cfs) and 1.7gpm/ft2 (0.21cfs). The OK 110 was tested at hydraulic loading rates of 4.8 and 8.1 gpm/ft2.

Average influent SSC for the SIL CO SIL 106 test runs 270mg/L. The average influent SSC was 211 and 424mg/L for the SIL CO SIL 250 influent at 3.2 and 1.7gpm respectively. The OK 110 tests calculated influent SSC ranged from 140-230mg/L with an average of 183.18. Field testing measured influent TSS at a mean 58mg/l.



# Isolator® Row O&M Manual









# THE ISOLATOR® ROW

#### INTRODUCTION

An important component of any Stormwater Pollution Prevention Plan is inspection and maintenance. The StormTech Isolator Row is a technique to inexpensively enhance Total Suspended Solids (TSS) removal and provide easy access for inspection and maintenance.

#### THE ISOLATOR ROW

The Isolator Row is a row of StormTech chambers, either SC-160LP, SC-310, SC-310-3, SC-740, DC-780, MC-3500 or MC-4500 models, that is surrounded with filter fabric and connected to a closely located manhole for easy access. The fabric-wrapped chambers provide for settling and filtration of sediment as storm water rises in the Isolator Row and ultimately passes through the filter fabric. The open bottom chambers and perforated sidewalls (SC-310, SC- 310-3 and SC-740 models) allow storm water to flow both vertically and horizontally out of the chambers. Sediments are captured in the Isolator Row protecting the storage areas of the adjacent stone and chambers from sediment accumulation.

Two different fabrics are used for the Isolator Row. A woven geotextile fabric is placed between the stone and the Isolator Row chambers. The tough geotextile provides a media for storm water filtration and provides a durable surface for maintenance operations. It is also designed to prevent scour of the underlying stone and remain intact during high pressure jetting. A non-woven fabric is placed over the chambers to provide a filter media for flows passing through the perforations in the sidewall of the chamber. The non-woven fabric is not required over the SC-160LP, DC-780, MC-3500 or MC-4500 models as these chambers do not have perforated side walls.

The Isolator Row is typically designed to capture the "first flush" and offers the versatility to be sized on a volume basis or flow rate basis. An upstream manhole not only provides access to the Isolator Row but typically includes a high flow weir such that storm water flowrates or volumes that exceed the capacity of the Isolator Row overtop the over flow weir and discharge through a manifold to the other chambers.

The Isolator Row may also be part of a treatment train. By treating storm water prior to entry into the chamber system, the service life can be extended and pollutants such as hydrocarbons can be captured. Pre-treatment best management practices can be as simple as deep sump catch basins, oil-water separators or can be innovative storm water treatment devices. The design of the treatment train and selection of pretreatment devices by the design engineer is often driven by regulatory requirements. Whether pretreatment is used or not, the Isolator Row is recommended by StormTech as an effective means to minimize maintenance requirements and maintenance costs.

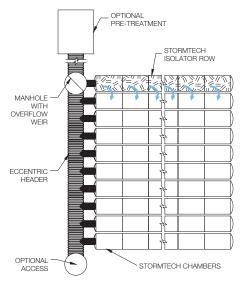
Note: See the StormTech Design Manual for detailed information on designing inlets for a StormTech system, including the Isolator Row.



Looking down the Isolator Row from the manhole opening, woven geotextile is shown between the chamber and stone base.



StormTech Isolator Row with Overflow Spillway (not to scale)





# ISOLATOR ROW INSPECTION/MAINTENANCE

#### **INSPECTION**

The frequency of inspection and maintenance varies by location. A routine inspection schedule needs to be established for each individual location based upon site specific variables. The type of land use (i.e. industrial, commercial, residential), anticipated pollutant load, percent imperviousness, climate, etc. all play a critical role in determining the actual frequency of inspection and maintenance practices.

At a minimum, StormTech recommends annual inspections. Initially, the Isolator Row should be inspected every 6 months for the first year of operation. For subsequent years, the inspection should be adjusted based upon previous observation of sediment deposition.

The Isolator Row incorporates a combination of standard manhole(s) and strategically located inspection ports (as needed). The inspection ports allow for easy access to the system from the surface, eliminating the need to perform a confined space entry for inspection purposes.

If upon visual inspection it is found that sediment has accumulated, a stadia rod should be inserted to determine the depth of sediment. When the average depth of sediment exceeds 3 inches throughout the length of the Isolator Row, clean-out should be performed.

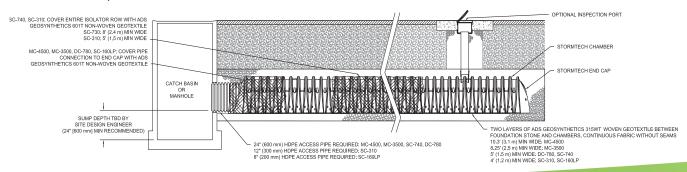
#### **MAINTENANCE**

The Isolator Row was designed to reduce the cost of periodic maintenance. By "isolating" sediments to just one row, costs are dramatically reduced by eliminating the need to clean out each row of the entire storage bed. If inspection indicates the potential need for maintenance, access is provided via a manhole(s) located on the end(s) of the row for cleanout. If entry into the manhole is required, please follow local and OSHA rules for a confined space entries.

Maintenance is accomplished with the JetVac process. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row while scouring and suspending sediments. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles. Selection of an appropriate JetVac nozzle will improve maintenance efficiency. Fixed nozzles designed for culverts or large diameter pipe cleaning are preferable. Rear facing jets with an effective spread of at least 45" are best. Most JetVac reels have 400 feet of hose allowing maintenance of an Isolator Row up to 50 chambers long. The JetVac process shall only be performed on StormTech Isolator Rows that have AASHTO class 1 woven geotextile (as specified by StormTech) over their angular base stone.

#### StormTech Isolator Row (not to scale)

Note: Non-woven fabric is only required over the inlet pipe connection into the end cap for SC-160LP, DC-780, MC-3500 and MC-4500 chamber models and is not required over the entire Isolator Row.





### ISOLATOR ROW STEP BY STEP MAINTENANCE PROCEDURES

#### STEP 1

Inspect Isolator Row for sediment.

- A) Inspection ports (if present)
  - i. Remove lid from floor box frame
  - ii. Remove cap from inspection riser
  - iii. Using a flashlight and stadia rod, measure depth of sediment and record results on maintenance log.
  - iv. If sediment is at or above 3 inch depth, proceed to Step 2. If not, proceed to Step 3.
- B) All Isolator Rows
  - i. Remove cover from manhole at upstream end of Isolator Row
  - ii. Using a flashlight, inspect down Isolator Row through outlet pipe
    - 1. Mirrors on poles or cameras may be used to avoid a confined space entry
    - 2. Follow OSHA regulations for confined space entry if entering manhole
  - iii. If sediment is at or above the lower row of sidewall holes (approximately 3 inches), proceed to Step 2. If not, proceed to Step 3.

#### STEP 2

Clean out Isolator Row using the JetVac process.

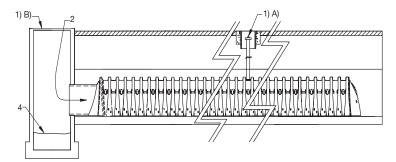
- A) A fixed floor cleaning nozzle with rear facing nozzle spread of 45 inches or more is preferable
- B) Apply multiple passes of JetVac until backflush water is clean
- C) Vacuum manhole sump as required

#### STEP 3

Replace all caps, lids and covers, record observations and actions.

#### STEP 4

Inspect & clean catch basins and manholes upstream of the StormTech system.



#### SAMPLE MAINTENANCE LOG

Stadia Rod Readings		Sediment Depth			
Date	Fixed point to chamber bottom (1)	Fixed point to top of sediment (2)	(1)-(2)	Observations/Actions	Inspector
3/15/11	6.3 ft	none		New installation. Fixed point is CI frame at grade	MCG
9/24/11		6.2	0.1 ft	Some grit felt	SM
6/20/13		5,8	o.s ft	Mucky feel, debris visible in manhole and in Isolator Row, maintenance due	Ν
7/7/13	6.3 ft		0	System jetted and vacuumed	MCG



